



Centre Tecnològic de Transferència de Calor
UNIVERSITAT POLITÈCNICA DE CATALUNYA



Proper SGS heat flux models for LES

F.Xavier Trias¹, Daniel Santos¹, Firas Dabbagh²,
Andrey Gorobets³, Assensi Oliva¹

¹Heat and Mass Transfer Technological Center, Technical University of Catalonia

²Christian-Doppler Laboratory for Multi-scale Modelling of Multiphase Processes,
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Contents

- 1 Motivation
- 2 On the modeling of SGS heat flux
- 3 Preserving symmetries at discrete level
- 4 Conclusions

Motivation

Research question #1:

- Can we find a nonlinear SGS heat flux model with **good physical** and **numerical properties**, such that we can obtain satisfactory predictions for a turbulent Rayleigh-Bénard convection?

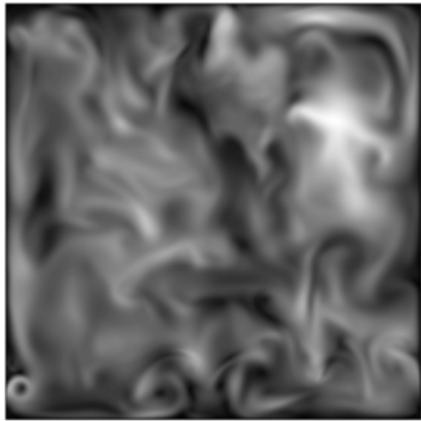
DNS of an air-filled Rayleigh-Bénard convection at $Ra = 10^{10}$

¹F.Dabbagh, F.X.Trias, A.Gorobets, A.Oliva. *On the evolution of flow topology in turbulent Rayleigh-Bénard convection*, **Physics of Fluids**, 28:115105, 2016.

Motivation

Air-filled RB: $Pr = 0.7$

$Ra = 10^8$

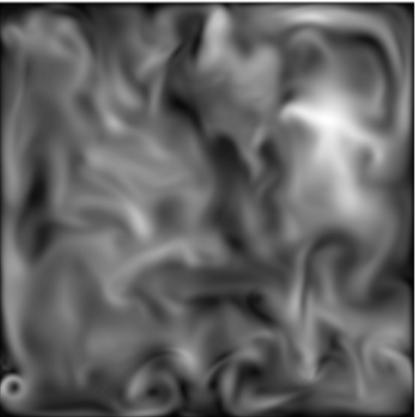


²F.Dabbagh, F.X.Trias, A.Gorobets, A.Oliva. *Flow topology dynamics in a 3D phase space for turbulent Rayleigh-Bénard convection*, **Phys.Rev.Fluids**, 5:024603, 2020.

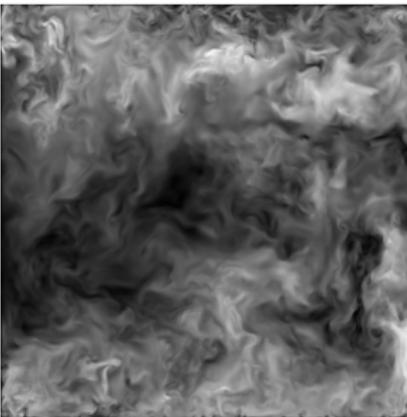
Motivation

Air-filled RB: $Pr = 0.7$

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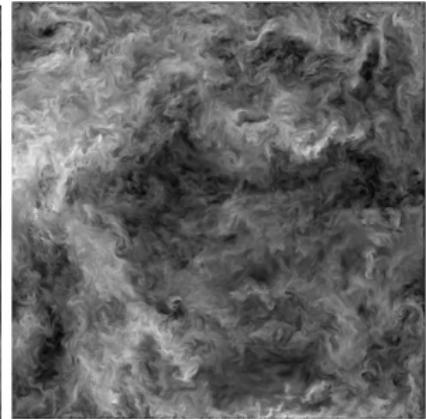
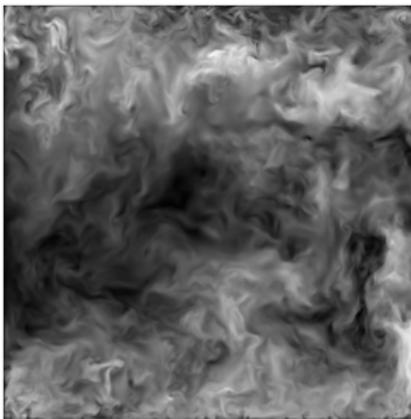
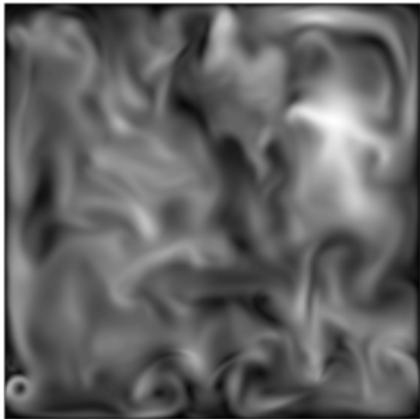


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Motivation

Air-filled RB: $Pr = 0.7$
 $Ra = 10^8$ $Ra = 10^{10}$

$Ra = 10^{11}$



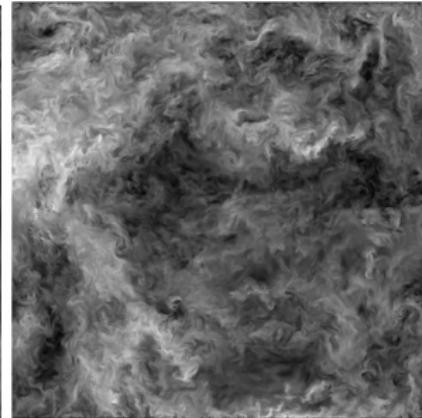
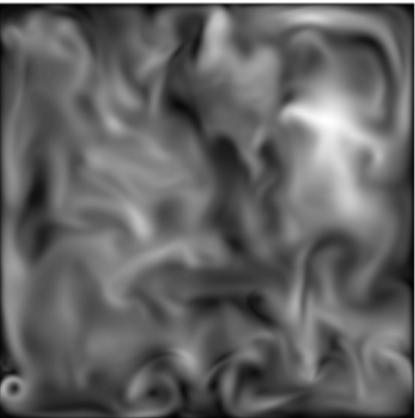
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Motivation

Air-filled RB: $Pr = 0.7$



$Ra = 10^8$



$Ra = 10^{10}$

$Ra = 10^{11}$

$208 \times 208 \times 400$
17.5M

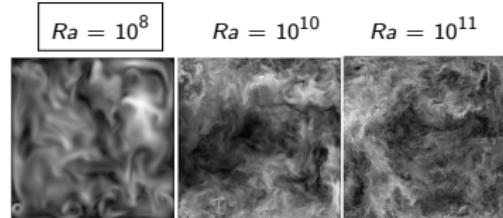
$768 \times 768 \times 1024$
607M

$1662 \times 1662 \times 2048$
5600M

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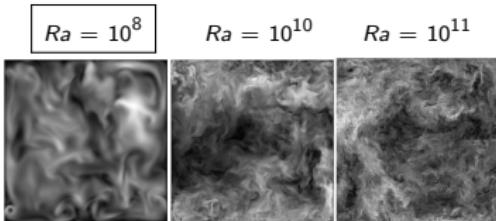
DNS: $208 \times 208 \times 400$



Motivation

DNS: $208 \times 208 \times 400$

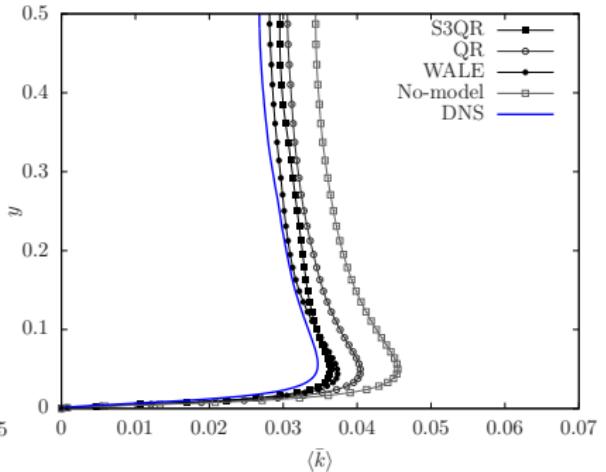
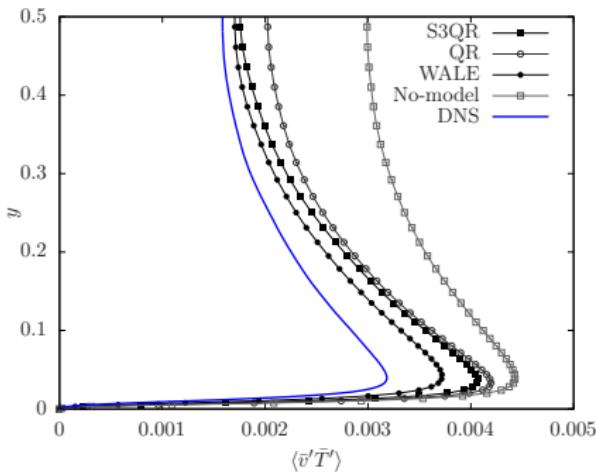
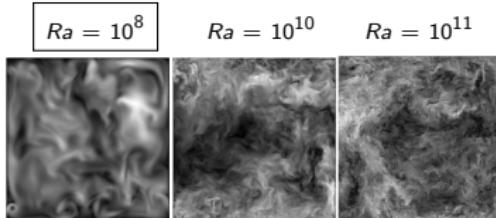
LES: $80 \times 80 \times 120$



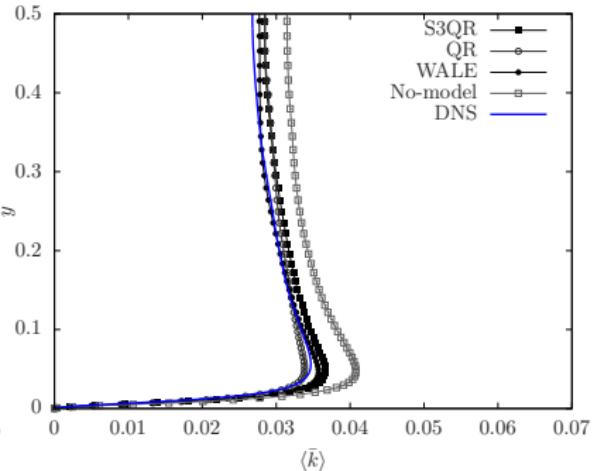
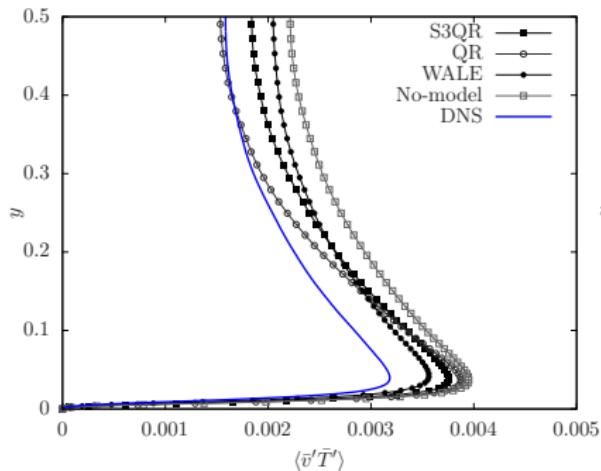
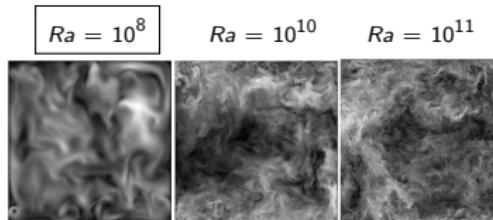
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LES: $80 \times 80 \times 120$



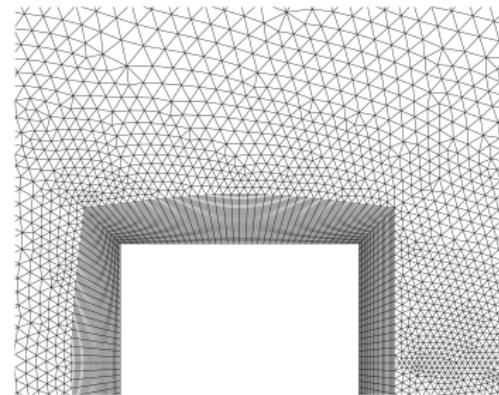
Motivation

DNS: $208 \times 208 \times 400$ LES: $110 \times 110 \times 168$ 

Motivation

Research question #2:

- Can we construct numerical discretizations of the Navier-Stokes equations suitable for **complex geometries**, such that the **symmetry properties** are exactly preserved?

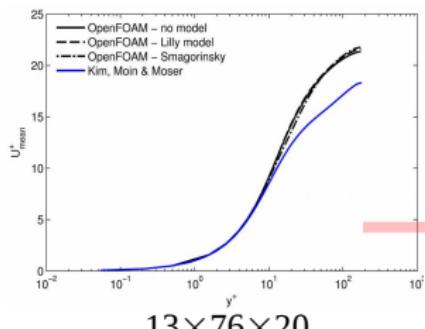


DNS³ of the turbulent flow around a square cylinder at $Re = 22000$

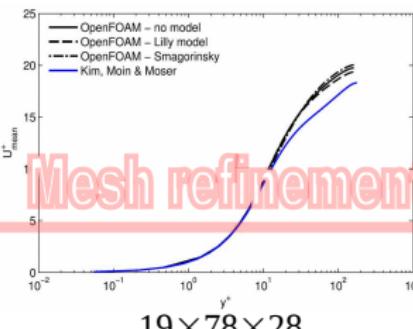
³F.X.Trias, A.Gorobets, A.Oliva. *Turbulent flow around a square cylinder at Reynolds number 22000: a DNS study*, **Computers&Fluids**, 123:87-98, 2015.

Motivation

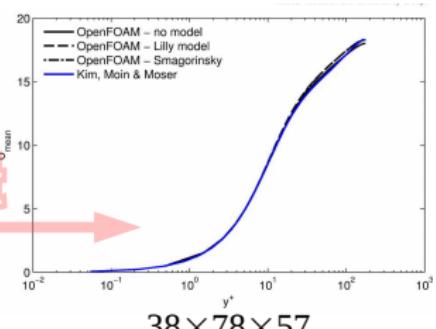
Open ∇ FOAM® LES⁴ results of a turbulent channel flow at $Re_\tau = 180$



$$\Delta x^+ = 90, \Delta y_{wall}^+ = 0.5, \Delta z^+ = 30$$



$$\Delta x^+ = 60, \Delta y_{wall}^+ = 0.5, \Delta z^+ = 20$$



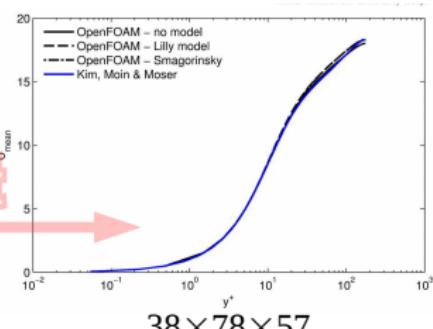
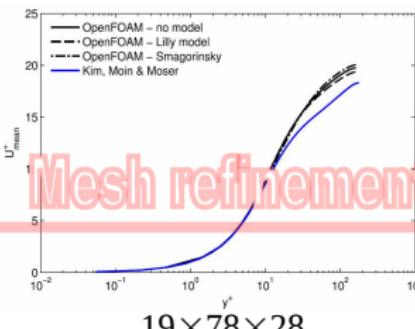
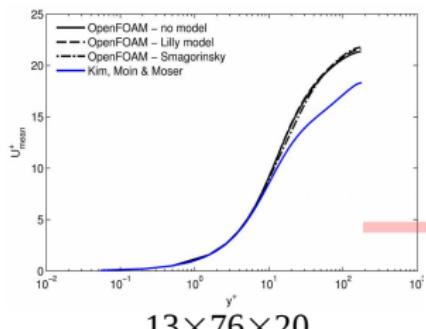
$$\Delta x^+ = 30, \Delta y_{wall}^+ = 0.5, \Delta z^+ = 10$$

Mesh refinement

⁴E.M.J.Komen, L.H.Camilo, A.Shams, B.J.Geurts, B.Koren. *A quantification method for numerical dissipation in quasi-DNS and under-resolved DNS, and effects of numerical dissipation in quasi-DNS and under-resolved DNS of turbulent channel flows*, **Journal of Computational Physics**, 345, 565-595, 2017.

Motivation

Open ∇ FOAM® LES⁴ results of a turbulent channel flow at $Re_\tau = 180$



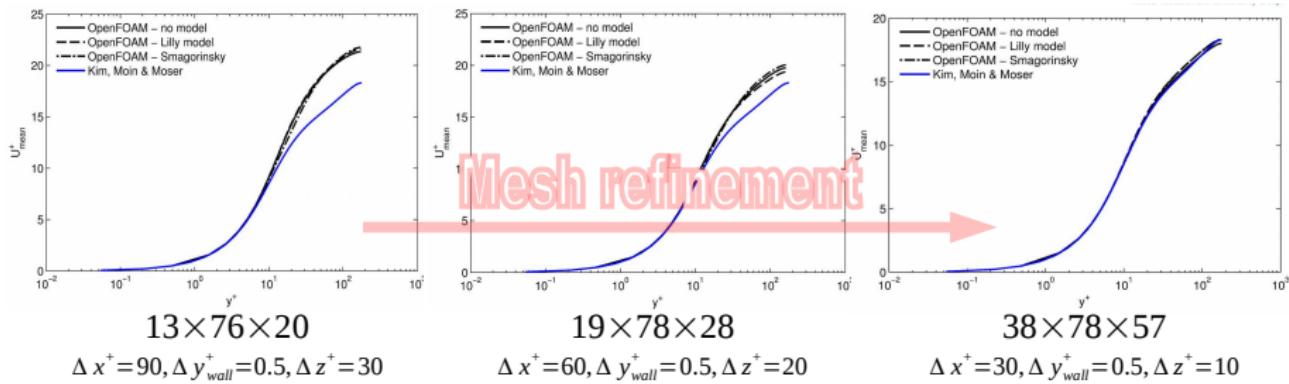
Mesh refinement

- Are LES results a merit of the SGS model?

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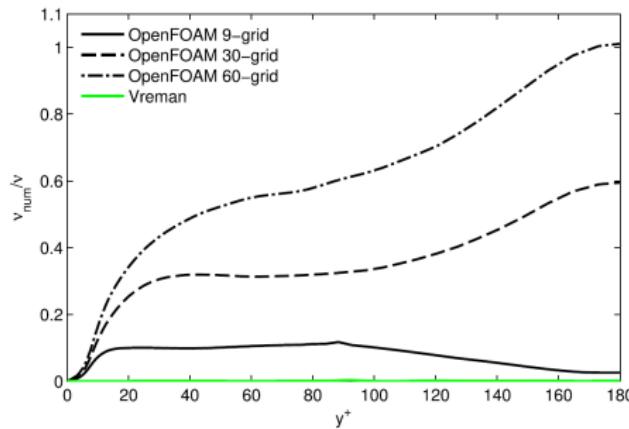
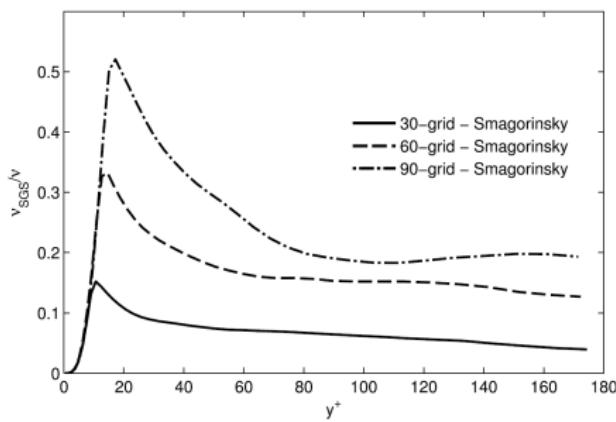


- Are LES results a merit of the SGS model? Apparently **NOT!!!** ✗

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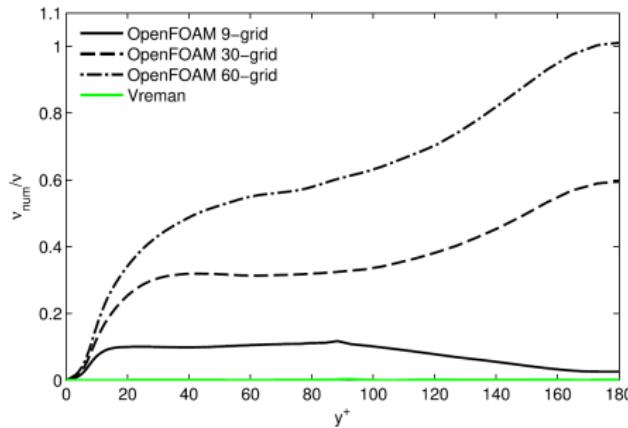
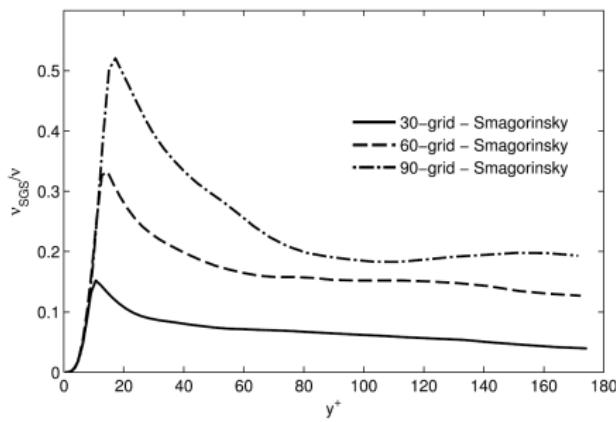


$$v_{num} \neq 0$$

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OpenFOAM® LES⁵ results of a turbulent channel flow at $Re_\tau = 180$



$$\nu_{SGS} < \nu_{num} \neq 0$$

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How to model the subgrid heat flux in LES?

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eddy-viscosity $\longrightarrow \tau(\bar{\mathbf{u}}) = -2\nu_t S(\bar{\mathbf{u}})$

$$\nu_t \approx (C_m \delta)^2 D_m(\bar{\mathbf{u}})$$

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$$\alpha_t = \frac{\nu_t}{Pr_t}$$

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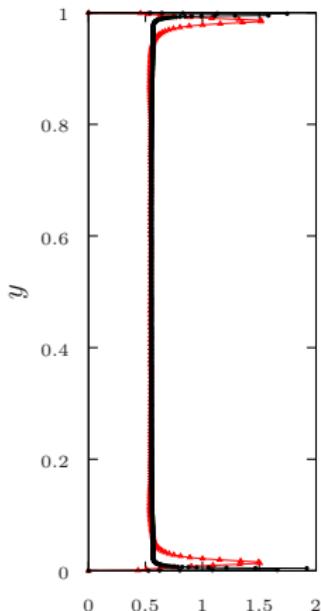
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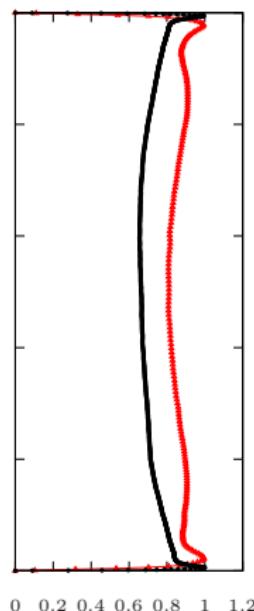
Pr_t ?

How to model the subgrid heat flux in LES?

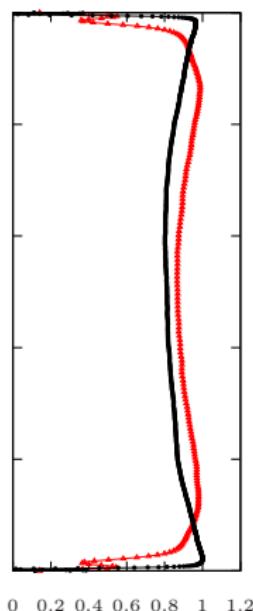
$$\begin{aligned} Ra = 10^8 & \quad \text{---} \bullet \\ Ra = 10^{10} & \quad \text{---} \circ \end{aligned}$$



$$Pr_t = \langle \nu_t \rangle_A / \langle \kappa_t \rangle_A$$



$$\langle \nu_t \rangle_A / \langle |\nu_{t,max}| \rangle_A$$



$$\langle \kappa_t \rangle_A / \langle |\kappa_{t,max}| \rangle_A$$

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$$G \equiv \nabla \bar{\mathbf{u}} \quad \mathbf{q} = -\frac{\delta^2}{12} G \nabla \bar{T} + \mathcal{O}(\delta^4)$$

A priori alignment trends⁶

$$\text{eddy-diffusivity} \longrightarrow \mathbf{q} \approx -\alpha_t \nabla \bar{T} \quad (\equiv \mathbf{q}^{\text{eddy}})$$

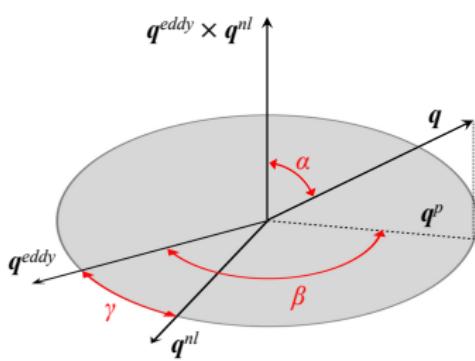
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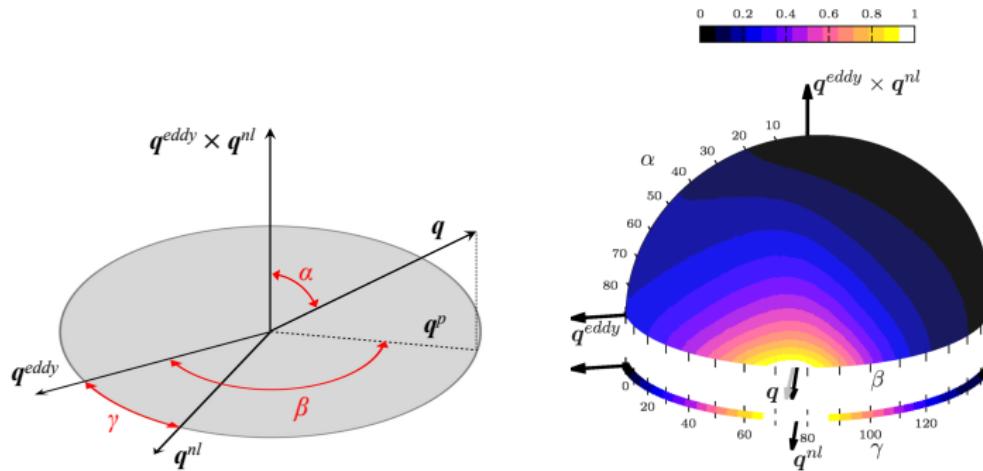


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eddy-diffusivity $\rightarrow \mathbf{q} \approx -\alpha_t \nabla \bar{T} \quad (\equiv \mathbf{q}^{\text{eddy}})$

gradient model $\rightarrow \mathbf{q} \approx -\frac{\delta^2}{12} G \nabla \bar{T} \quad (\equiv \mathbf{q}^{nl})$

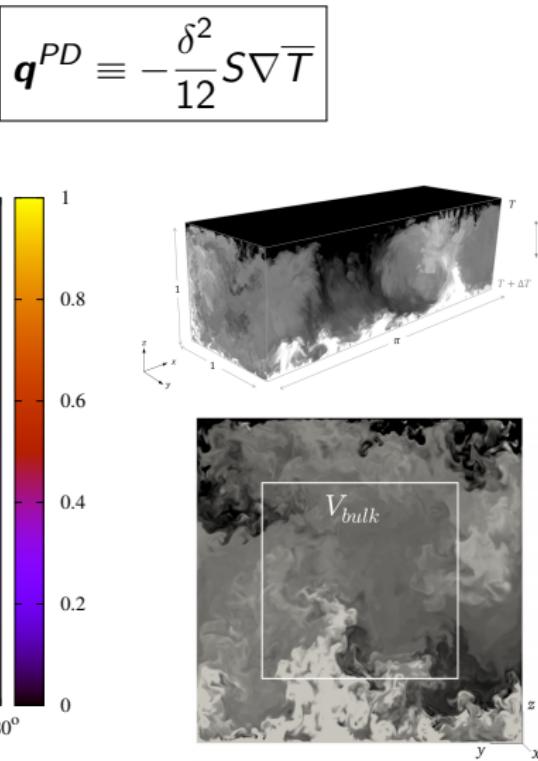
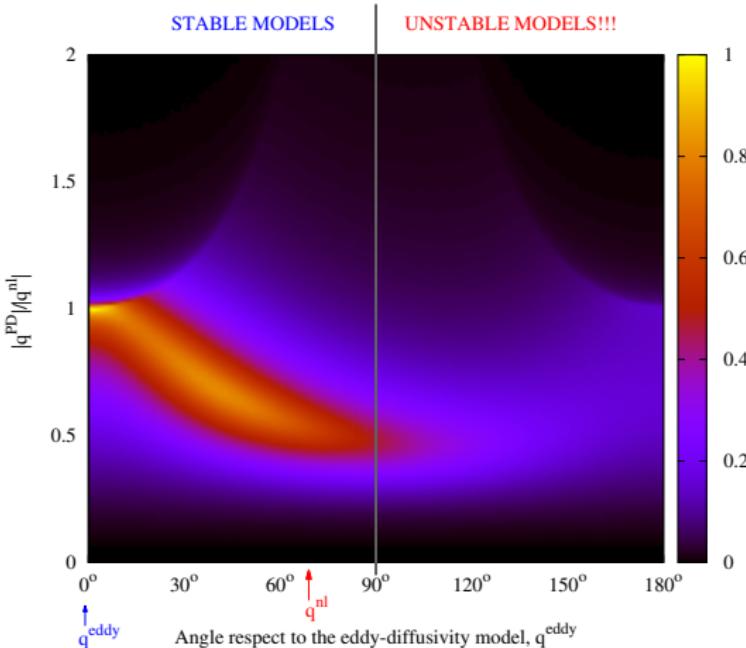
Peng&Davidson⁷ $\rightarrow \mathbf{q} \approx -\frac{\delta^2}{12} S \nabla \bar{T} \quad (\equiv \mathbf{q}^{PD})$

⁷S.Peng and L.Davidson. **Int.J.Heat Mass Transfer**, 45:1393-1405, 2002.

A priori alignment trends

$$\mathbf{q}^{nl} \equiv -\frac{\delta^2}{12} G \nabla \bar{T}$$

$$\mathbf{q}^{PD} \equiv -\frac{\delta^2}{12} S \nabla \bar{T}$$



How to model the subgrid heat flux in LES?

$$\partial_t \bar{\mathbf{u}} + (\bar{\mathbf{u}} \cdot \nabla) \bar{\mathbf{u}} = \nu \nabla^2 \bar{\mathbf{u}} - \nabla \bar{p} + \bar{\mathbf{f}} - \nabla \cdot \tau(\bar{\mathbf{u}}) ; \quad \nabla \cdot \bar{\mathbf{u}} = 0$$

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⁸B.J.Daly and F.H.Harlow. **Physics of Fluids**, 13:2634, 1970.

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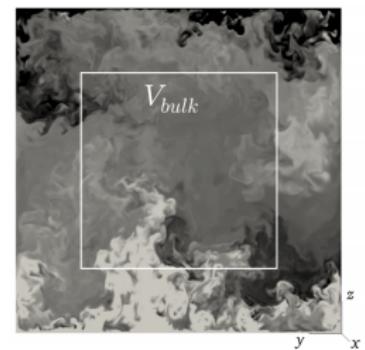
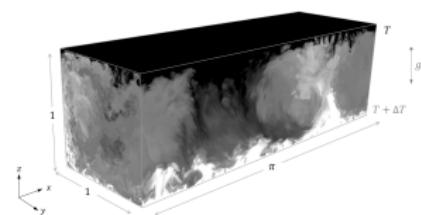
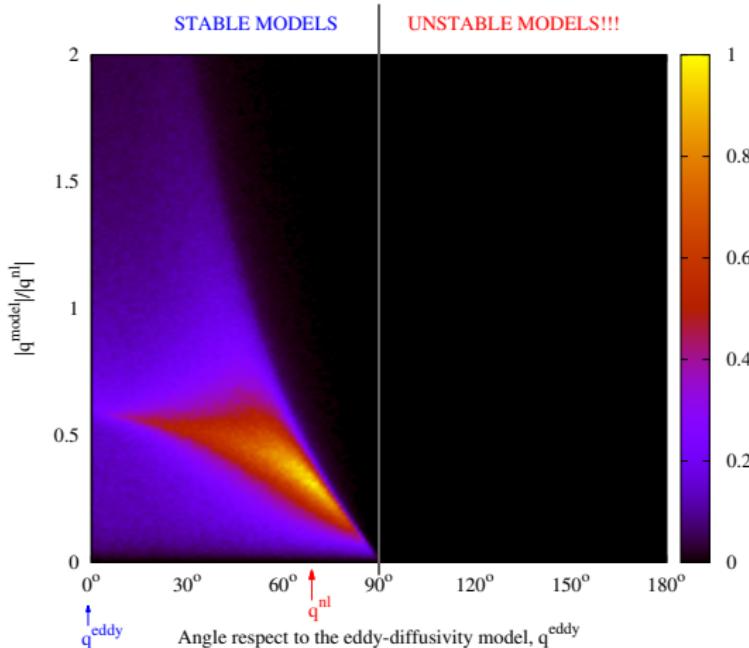
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A priori alignment trends

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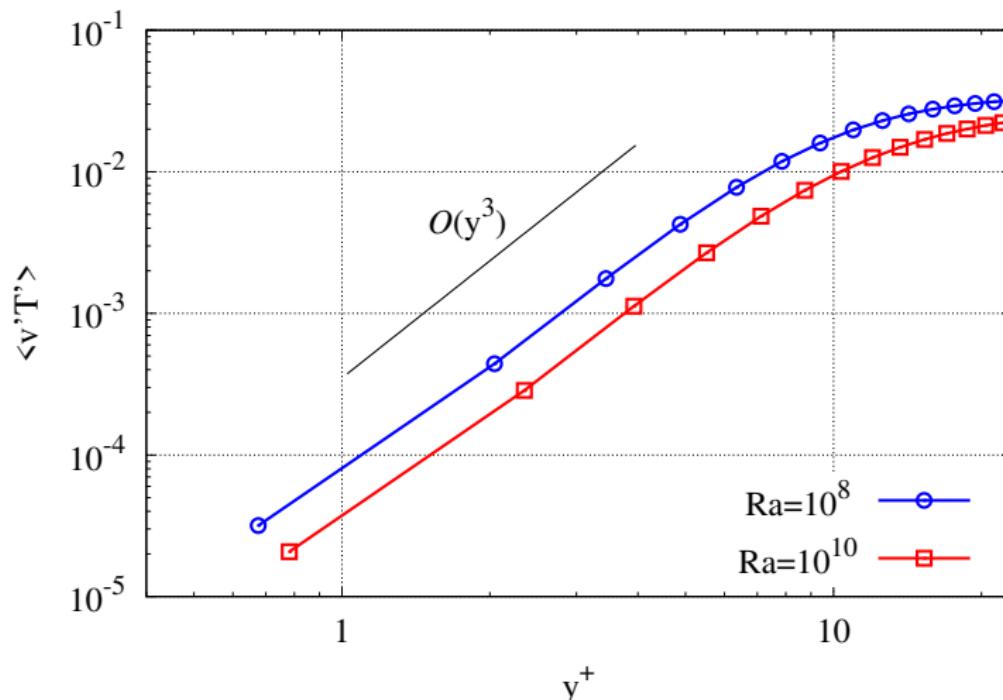
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What about near-wall scaling?

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⇒ Answer: it should be $\mathcal{O}(y^3)$



Near-wall scaling for DH model?

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Near-wall scaling for DH model?

⇒ Answer: it is $\mathcal{O}(y^1)$ instead of $\mathcal{O}(y^3)$

$$\mathbf{q}^{DH} \equiv -\mathcal{T}_{SGS} \frac{\delta^2}{12} \mathbf{G} \mathbf{G}^T \nabla \bar{T}; \quad \mathcal{T}_{SGS} = 1/|S|$$

$$u = ay + \mathcal{O}(y^2); \quad v = by^2 + \mathcal{O}(y^3); \quad w = cy + \mathcal{O}(y^2); \quad T = dy + \mathcal{O}(y^2)$$

$$G = \begin{pmatrix} y & 1 & y \\ y^2 & y & y^2 \\ y & 1 & y \end{pmatrix}; \quad \nabla \bar{T} = \begin{pmatrix} y \\ 1 \\ y \end{pmatrix} \implies \mathbf{G} \mathbf{G}^T \nabla \bar{T} = \begin{pmatrix} y \\ y^2 \\ y \end{pmatrix} = \mathcal{O}(y^1)$$

$$\mathcal{T}_{SGS} = 1/|S| = \mathcal{O}(y^0)$$

Near-wall scaling for DH model?

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$$\mathcal{T}_{SGS} = 1/|S| = \mathcal{O}(y^0)$$

Idea: build a \mathcal{T}_{SGS} with the proper $\mathcal{O}(y^2)$ scaling!!!

Building proper models for the subgrid heat flux⁹

Let us consider models that are based on the invariants of the tensor GG^T

$$\mathbf{q} \approx -C_M \left(P_{GG^T}^p Q_{GG^T}^q R_{GG^T}^r \right) \frac{\delta^2}{12} GG^T \nabla \bar{T} \quad (\equiv \mathbf{q}^{S2})$$

⁹F.X.Trias, F.Dabbagh, A.Gorobets, C.Oliet. *On a proper tensor-diffusivity model for LES of buoyancy-driven turbulence*, **Flow Turbul Combust**, 105:393-414, 2020.

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	P_{GG^T}	Q_{GG^T}	R_{GG^T}
Formula	$2(Q_\Omega - Q_S)$	$V^2 + Q_G^2$	R_G^2
Wall-behavior	$\mathcal{O}(y^0)$	$\mathcal{O}(y^2)$	$\mathcal{O}(y^6)$
Units	$[T^{-2}]$	$[T^{-4}]$	$[T^{-6}]$

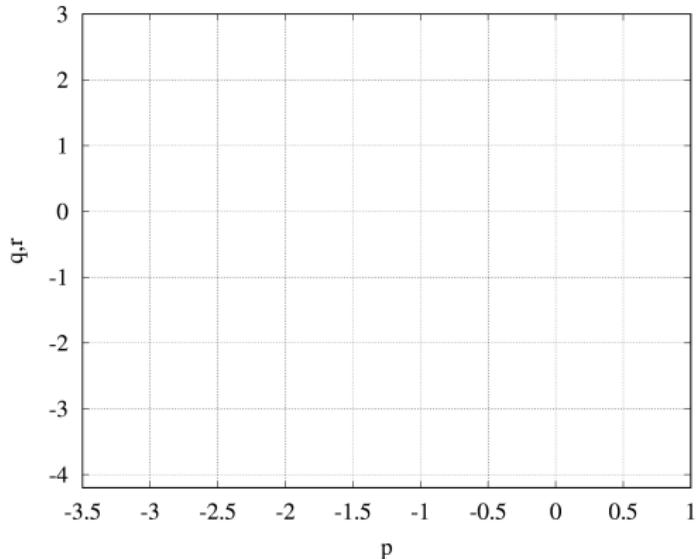
$$-6\mathbf{r} - 4\mathbf{q} - 2\mathbf{p} = 1 \quad [T]; \quad 6\mathbf{r} + 2\mathbf{q} = s,$$

where s is the slope for the asymptotic near-wall behavior, i.e. $\mathcal{O}(y^s)$.

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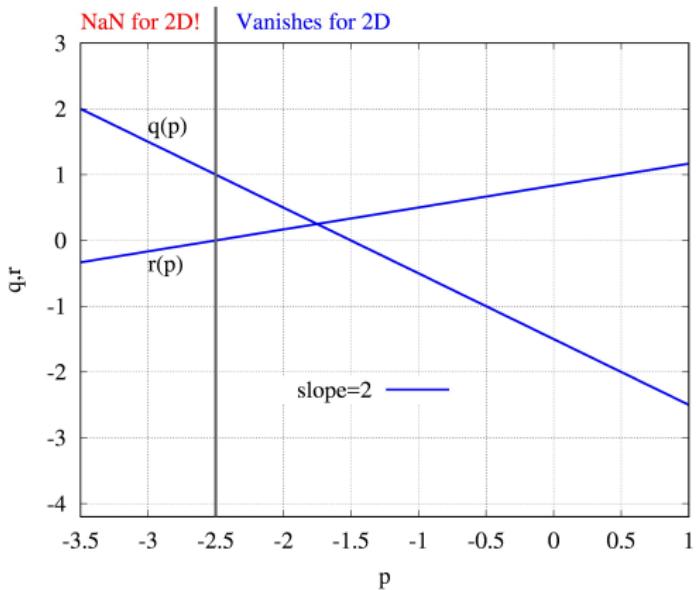
Solutions: $q(p, s) = -(1 + s)/2 - p$ and $r(p, s) = (2s + 1)/6 + p/3$



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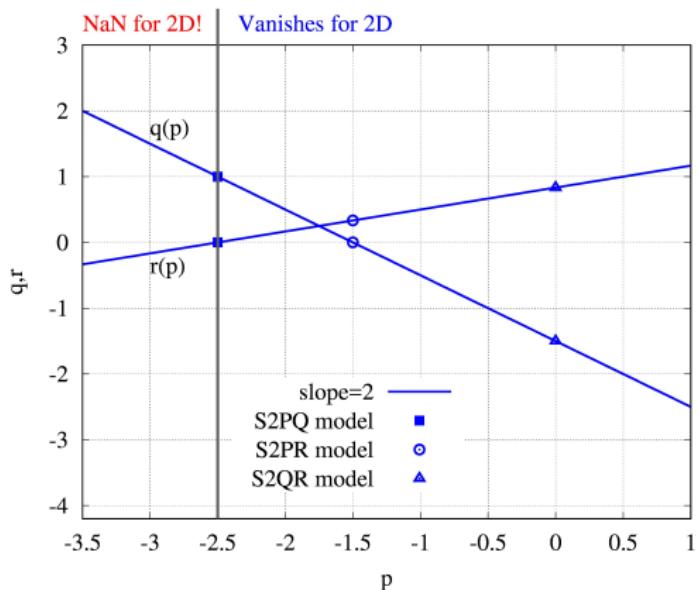
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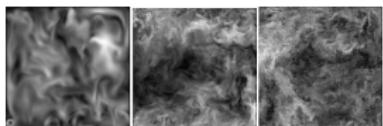
A priori analysis in the bulk

Estimation of the model constant, C_{s2pqr}

Playing with exponent p ...

$$\mathbf{q}^{S2PQR} \approx -C_{s2pqr} \left(P_{GG^T}^p Q_{GG^T}^{-(p+3/2)} R_{GG^T}^{(2p+5)/6} \right) \frac{\delta^2}{12} GG^T \nabla \bar{T}$$

$$Ra = 10^8 \quad Ra = 10^{10} \quad Ra = 10^{11}$$



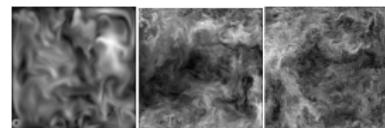
$$\frac{<|\mathbf{q}^{S2PQR}|>_{bulk}}{<|\mathbf{q}|>_{bulk}} = 1 \longrightarrow C_{s2pqr}$$

A priori analysis in the bulk

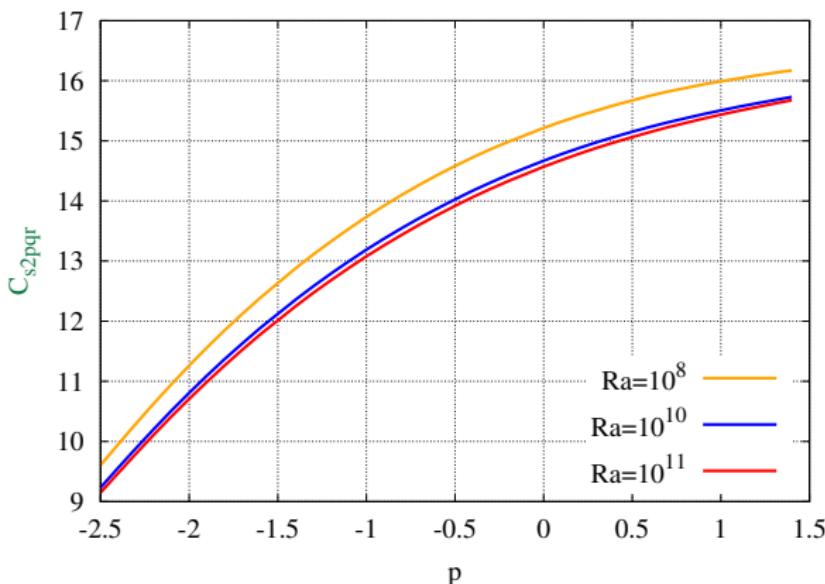
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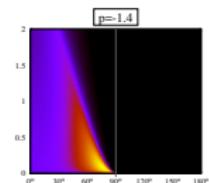
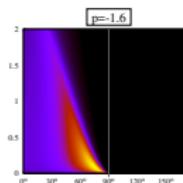
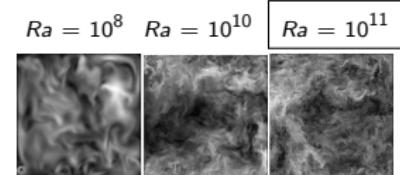
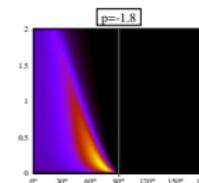
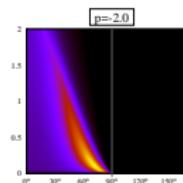
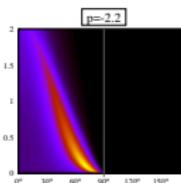
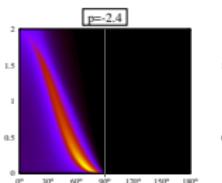


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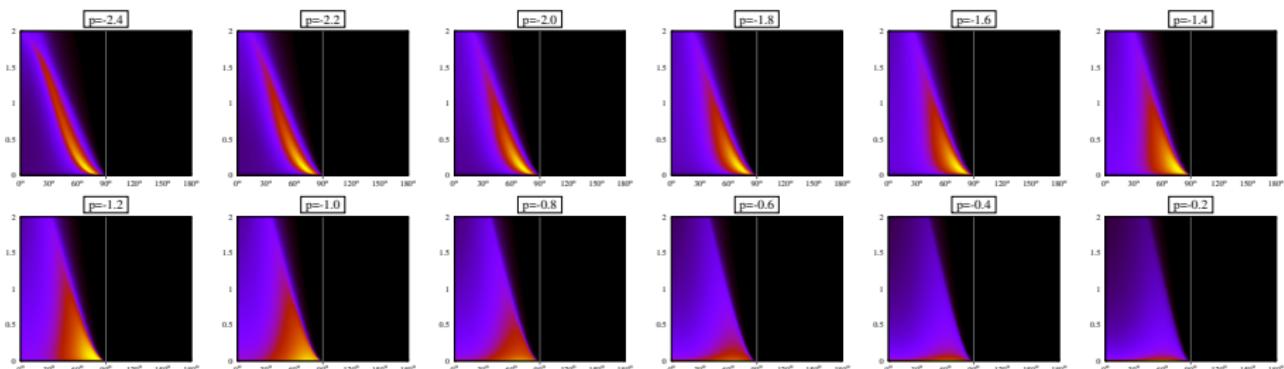


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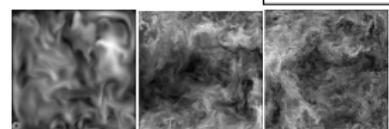
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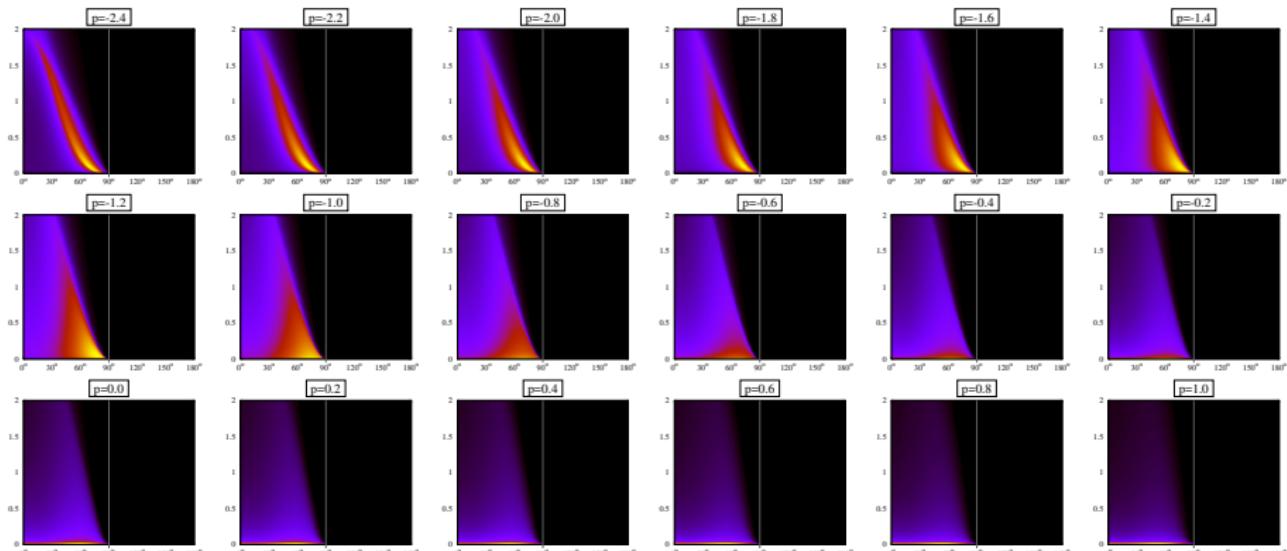


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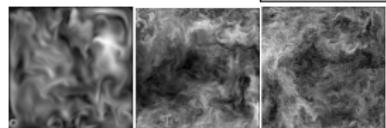
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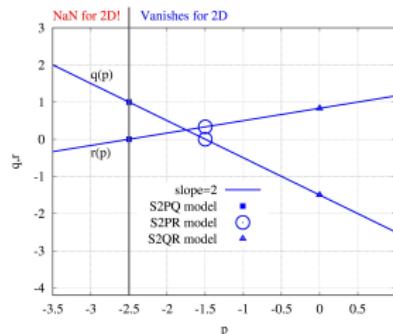
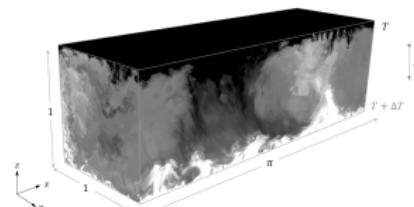
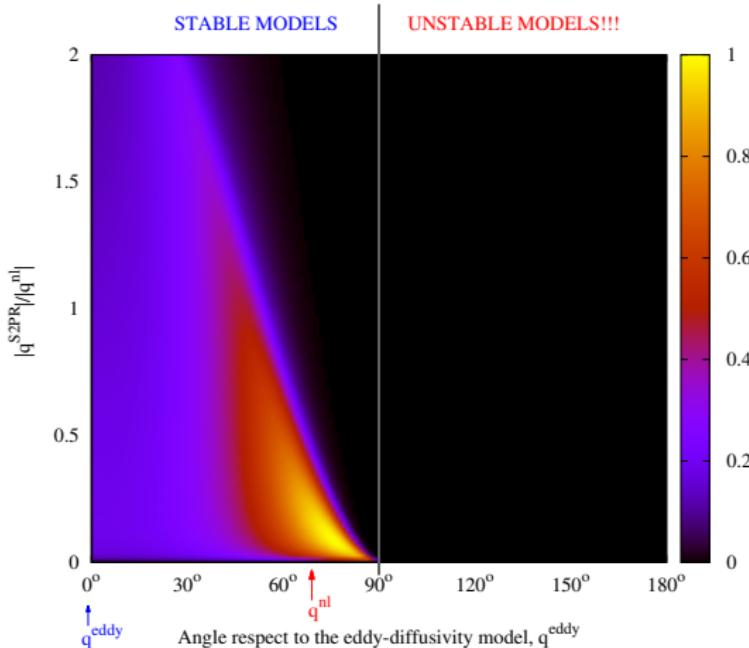
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A priori alignment trends of S2PR in the bulk

$$\mathbf{q}^{nl} \equiv -\frac{\delta^2}{12} G \nabla \bar{T}$$

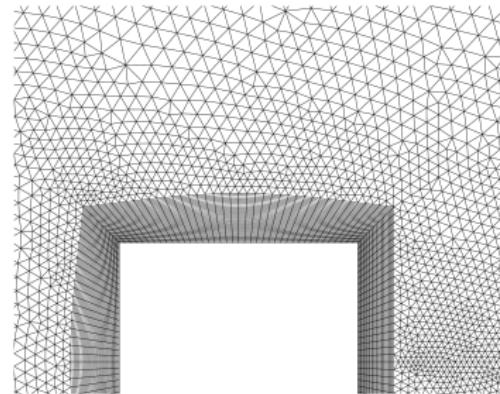
$$\mathbf{q}^{s2PR} \equiv -C_{s2pr} P_{GG^T}^{-3/2} R_{GG^T}^{1/3} \frac{\delta^2}{12} GG^T \nabla \bar{T}$$



Motivation

Research question #2:

- Can we construct numerical discretizations of the Navier-Stokes equations suitable for **complex geometries**, such that the **symmetry properties** are exactly preserved?



DNS³ of the turbulent flow around a square cylinder at $Re = 22000$

³F.X.Trias, A.Gorobets, A.Oliva. *Turbulent flow around a square cylinder at Reynolds number 22000: a DNS study*, **Computers&Fluids**, 123:87-98, 2015.

Symmetry-preserving discretization

Continuous

$$\frac{\partial \mathbf{u}}{\partial t} + \mathcal{C}(\mathbf{u}, \mathbf{u}) = \nu \nabla^2 \mathbf{u} - \nabla p$$

$$\nabla \cdot \mathbf{u} = 0$$

Symmetry-preserving discretization

Continuous

$$\frac{\partial \mathbf{u}}{\partial t} + \mathcal{C}(\mathbf{u}, \mathbf{u}) = \nu \nabla^2 \mathbf{u} - \nabla p$$

$$\nabla \cdot \mathbf{u} = 0$$

Discrete

$$\Omega \frac{d \mathbf{u}_h}{dt} + \mathcal{C}(\mathbf{u}_h) \mathbf{u}_h = \mathbf{D} \mathbf{u}_h - \mathbf{G} \mathbf{p}_h$$

$$\mathbf{M} \mathbf{u}_h = \mathbf{0}_h$$

Symmetry-preserving discretization

Continuous

$$\frac{\partial \mathbf{u}}{\partial t} + \mathcal{C}(\mathbf{u}, \mathbf{u}) = \nu \nabla^2 \mathbf{u} - \nabla p$$
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$$\langle \mathbf{a}, \mathbf{b} \rangle = \int_{\Omega} \mathbf{a} \mathbf{b} d\Omega$$

Discrete

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$$\langle \mathbf{a}_h, \mathbf{b}_h \rangle_h = \mathbf{a}_h^T \Omega \mathbf{b}_h$$

Symmetry-preserving discretization

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$$\Omega \frac{d \mathbf{u}_h}{dt} + \mathcal{C}(\mathbf{u}_h) \mathbf{u}_h = \mathbf{D} \mathbf{u}_h - \mathbf{G} \mathbf{p}_h$$

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$$\langle \mathbf{a}_h, \mathbf{b}_h \rangle_h = \mathbf{a}_h^T \Omega \mathbf{b}_h$$

$$\mathcal{C}(\mathbf{u}_h) = -\mathcal{C}^T(\mathbf{u}_h)$$

Symmetry-preserving discretization

Continuous

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$$\begin{aligned}\langle \mathcal{C}(\mathbf{u}, \varphi_1), \varphi_2 \rangle &= - \langle \mathcal{C}(\mathbf{u}, \varphi_2), \varphi_1 \rangle \\ \langle \nabla \cdot \mathbf{a}, \varphi \rangle &= - \langle \mathbf{a}, \nabla \varphi \rangle\end{aligned}$$

Discrete

$$\Omega \frac{d \mathbf{u}_h}{dt} + \mathcal{C}(\mathbf{u}_h) \mathbf{u}_h = \mathbf{D} \mathbf{u}_h - \mathbf{G} \mathbf{p}_h$$

$$\mathbf{M} \mathbf{u}_h = \mathbf{0}_h$$

$$\langle \mathbf{a}_h, \mathbf{b}_h \rangle_h = \mathbf{a}_h^T \Omega \mathbf{b}_h$$

$$\begin{aligned}\mathcal{C}(\mathbf{u}_h) &= -\mathcal{C}^T(\mathbf{u}_h) \\ \Omega \mathbf{G} &= -\mathbf{M}^T\end{aligned}$$

Symmetry-preserving discretization

Continuous

$$\frac{\partial \mathbf{u}}{\partial t} + \mathcal{C}(\mathbf{u}, \mathbf{u}) = \nu \nabla^2 \mathbf{u} - \nabla p$$

$$\nabla \cdot \mathbf{u} = 0$$

$$\langle \mathbf{a}, \mathbf{b} \rangle = \int_{\Omega} \mathbf{a} \mathbf{b} d\Omega$$

$$\langle \mathcal{C}(\mathbf{u}, \varphi_1), \varphi_2 \rangle = - \langle \mathcal{C}(\mathbf{u}, \varphi_2), \varphi_1 \rangle$$

$$\langle \nabla \cdot \mathbf{a}, \varphi \rangle = - \langle \mathbf{a}, \nabla \varphi \rangle$$

$$\langle \nabla^2 \mathbf{a}, \mathbf{b} \rangle = - \langle \mathbf{a}, \nabla^2 \mathbf{b} \rangle$$

Discrete

$$\Omega \frac{d \mathbf{u}_h}{dt} + \mathcal{C}(\mathbf{u}_h) \mathbf{u}_h = \mathbf{D} \mathbf{u}_h - \mathbf{G} \mathbf{p}_h$$

$$\mathbf{M} \mathbf{u}_h = \mathbf{0}_h$$

$$\langle \mathbf{a}_h, \mathbf{b}_h \rangle_h = \mathbf{a}_h^T \Omega \mathbf{b}_h$$

$$\mathcal{C}(\mathbf{u}_h) = -\mathcal{C}^T(\mathbf{u}_h)$$

$$\Omega \mathbf{G} = -\mathbf{M}^T$$

$$\mathbf{D} = \mathbf{D}^T \quad def -$$

Why collocated arrangements are so popular?

- STAR-CCM+



SIEMENS

- ANSYS-FLUENT



- Code-Saturne



- OpenFOAM



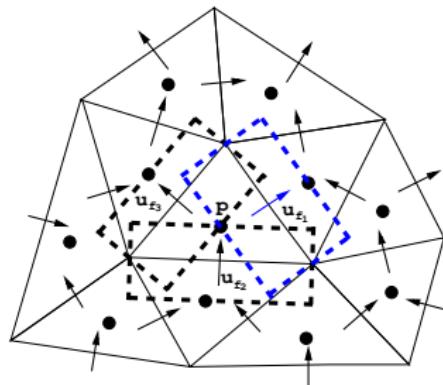
GPL



$$\Omega_s \frac{d\mathbf{u}_s}{dt} + C(\mathbf{u}_s) \mathbf{u}_s = D\mathbf{u}_s - G\mathbf{p}_c; \quad M\mathbf{u}_s = \mathbf{0}_c$$

In staggered meshes

- $p-\mathbf{u}_s$ coupling is naturally solved ✓
- $C(\mathbf{u}_s)$ and D difficult to discretize ✗



Why collocated arrangements are so popular?

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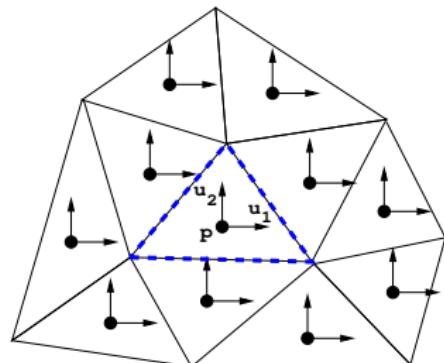
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In collocated meshes

- $p-\mathbf{u}_c$ coupling is cumbersome **X**
- $\mathbf{C}(\mathbf{u}_s)$ and \mathbf{D} easy to discretize **✓**
- Cheaper, less memory,... **✓**



Why collocated arrangements are so popular?

Everything is easy except the pressure-velocity coupling...

- STAR-CCM+



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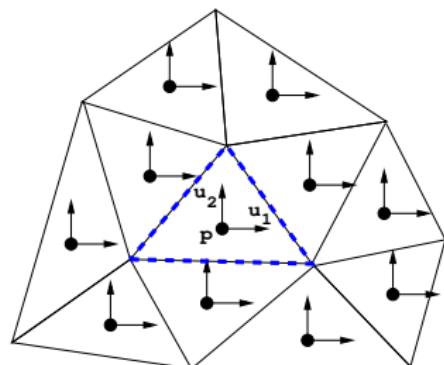
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Pressure-velocity coupling on collocated grids

A vicious circle that cannot be broken...

In summary¹⁰:

- Mass: $M\Gamma_{c \rightarrow s} u_c = M\Gamma_{c \rightarrow s} u_c - L_c L^{-1} M\Gamma_{c \rightarrow s} u_c \approx 0_c \times$
- Energy: $p_c (L - L_c) p_c \neq 0 \times$

↳ www.cfd-direct.com/2014/01/preserving-symmetries-at-discrete-level.html

¹⁰ F.X.Trias, O.Lehmkuhl, A.Oliva, C.D.Pérez-Segarra, R.W.C.P.Verstappen.
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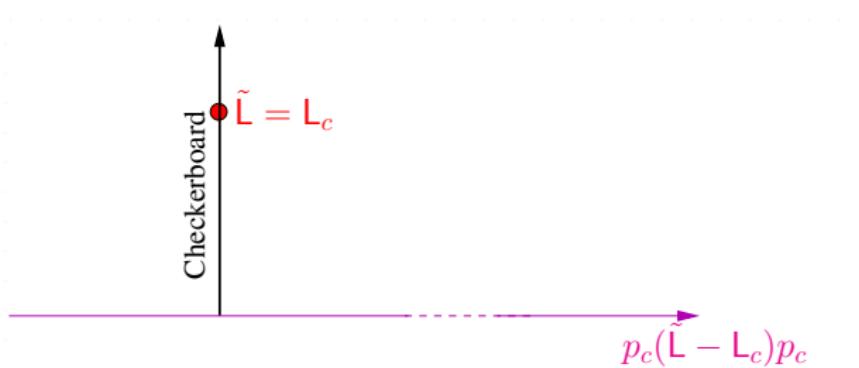
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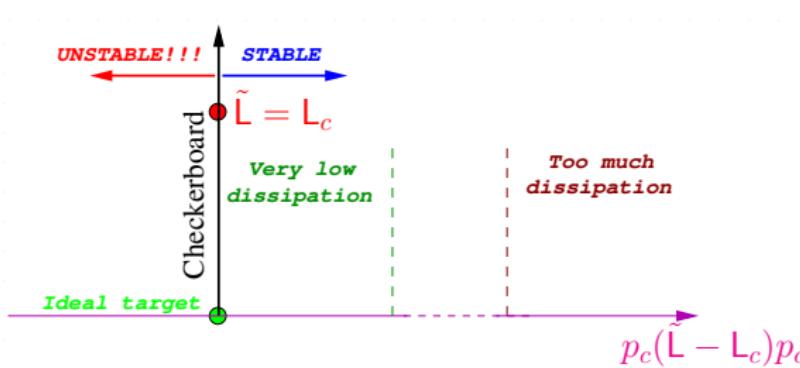
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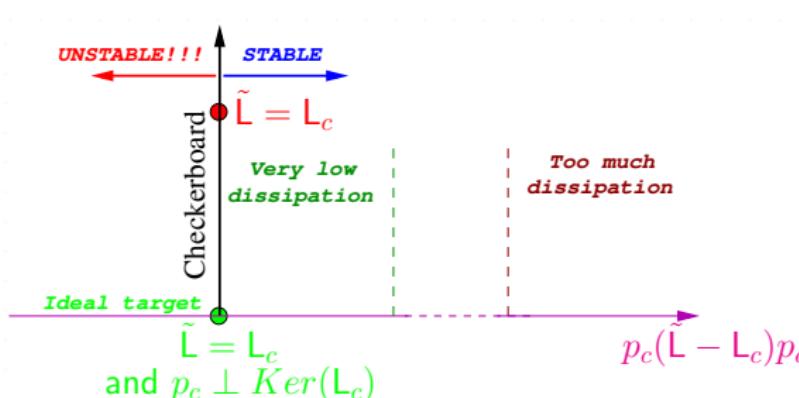
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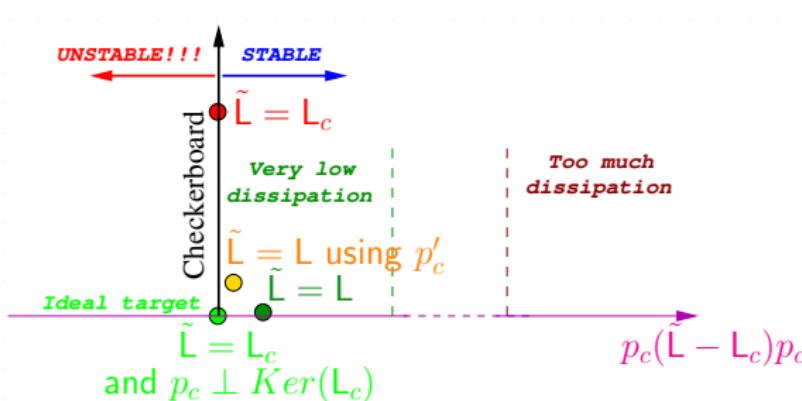
¹⁰Shashank, J.Larsson, G.Iaccarino. *A co-located incompressible Navier-Stokes solver with exact mass, momentum and kinetic energy conservation in the inviscid limit*, Journal of Computational Physics, 229: 4425-4430,2010.

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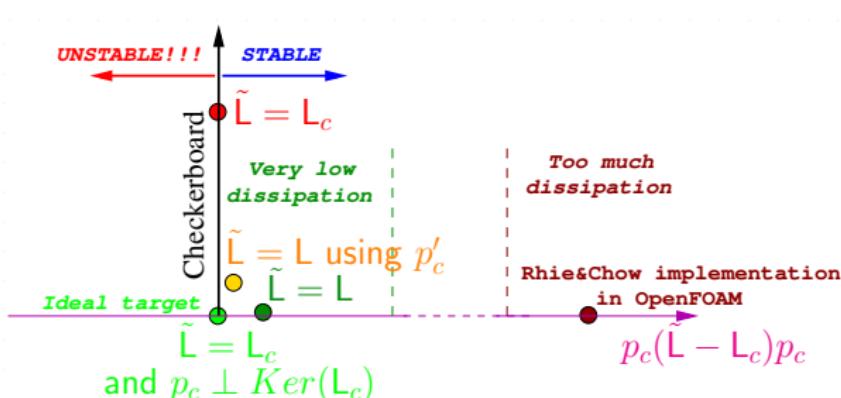
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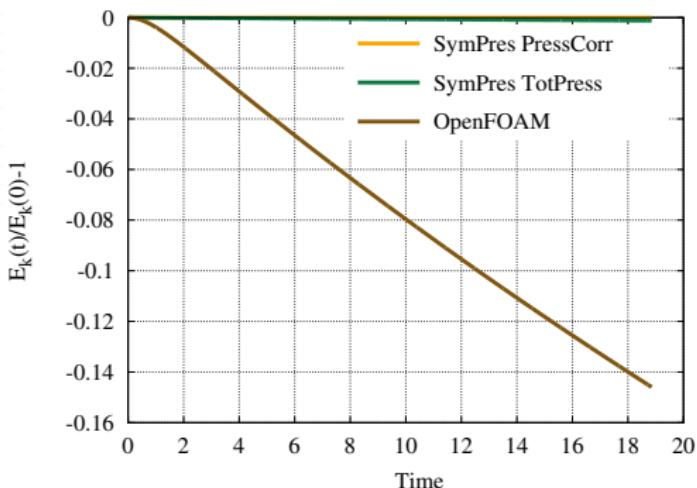
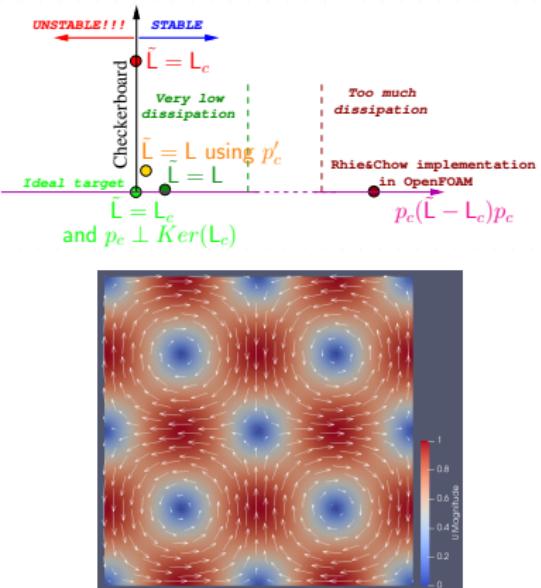
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Pressure-velocity coupling on collocated grids

A vicious circle that ~~cannot be broken~~ can almost be broken...

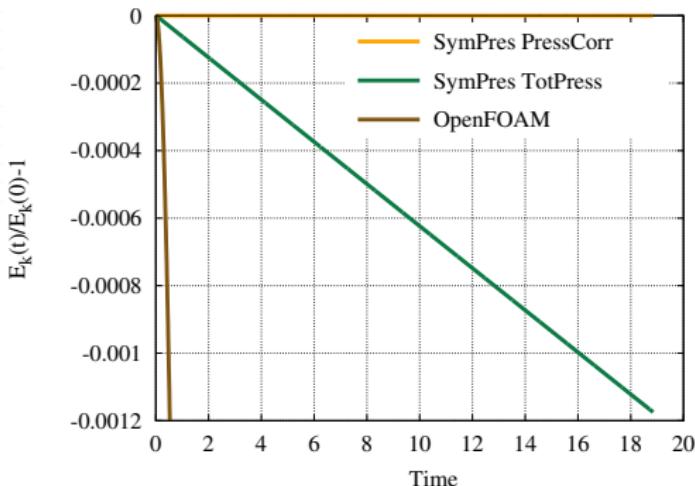
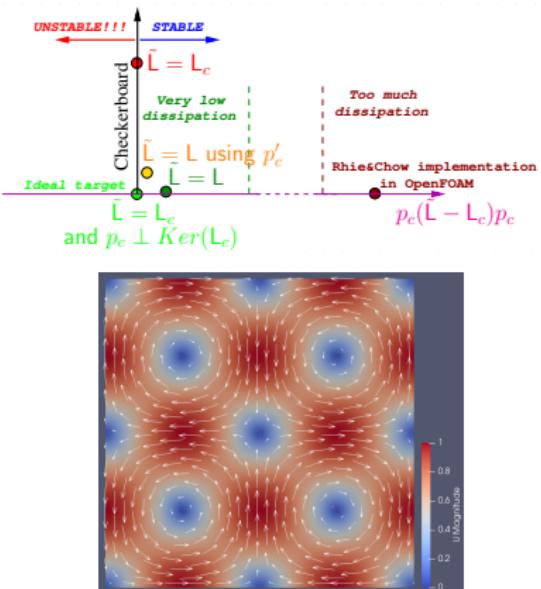


Results for an inviscid Taylor-Green vortex¹¹

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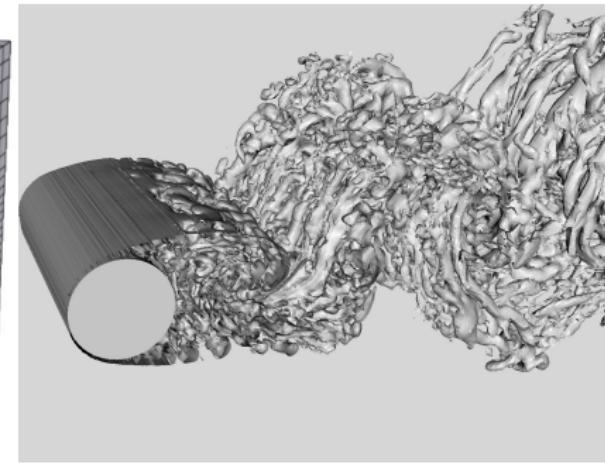
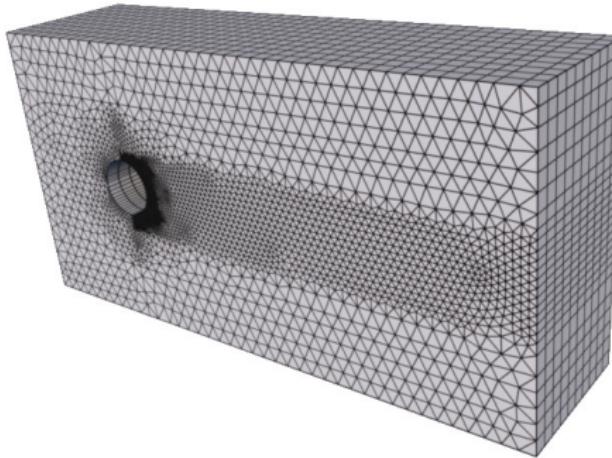
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Examples of simulations

Despite these inherent limitations, symmetry-preserving collocated formulation has been successfully used for DNS/LES simulations¹²:

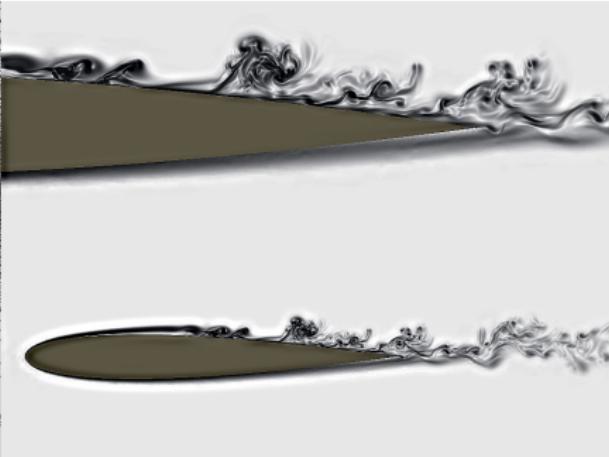
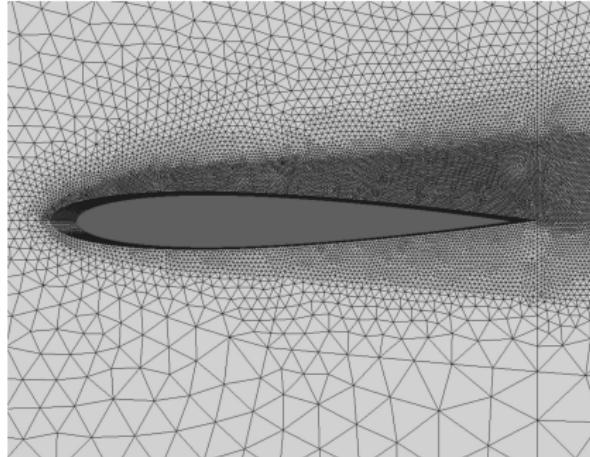


¹²R.Borrell, O.Lehmkuhl, F.X.Trias, A.Oliva. *Parallel Direct Poisson solver for discretizations with one Fourier diagonalizable direction.* **Journal of Computational Physics**, 230:4723-4741, 2011.

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Concluding remarks

- A new tensor-diffusivity model has been proposed

$$\mathbf{q}^{s2PR} \equiv -C_{s2pr} P_{GG^T}^{-3/2} R_{GG^T}^{1/3} \frac{\delta^2}{12} GG^T \nabla \bar{T}$$

- Locally defined, unconditionally stable and vanishes for 2D flows ✓
- Good *a priori* alignment trends and proper near-wall scaling ✓

¹³On Friday at **16:50 in Room B**: N.Valle, F.X.Trias, R.W.C.P.Verstappen.
Symmetry-preserving discretizations in unstructured staggered meshes

¹⁴On Friday at **10:50 in Room A**: A.P.Duben, J.Ruano, J.Rigola, F.X.Trias.
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Future research:

- *A posteriori* tests using \mathbf{q}^{s2PR} for RB

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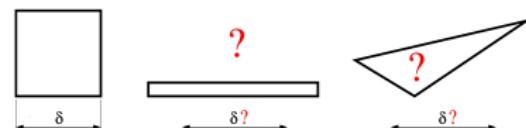
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- Definition of δ for anisotropic grids^{14?}



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Thank you for your
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Acknowledgements



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