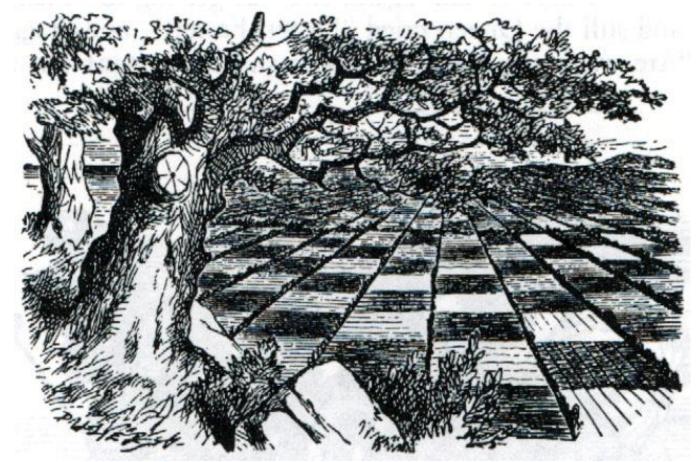
AN UNCONDITIONALLY STABLE, ENERGY PRESERVING METHOD FOR MAGNETOHYDRODYNAMICS

J.A. Hopman, J. Rigola, F.X. Trias

<u>D. Santos</u>











Motivation

MagnetoHydroDynamic (MHD) flows for Nuclear Fusion





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-High Hartmann number,

$$Ha = LB_0 \sqrt{\frac{\sigma_0}{\rho_0 \nu}}$$





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-High Hartmann number,

$$Ha = LB_0 \sqrt{\frac{\sigma_0}{\rho_0 \nu}}$$
$$Re_m = \sigma \mu Lu_0 \ll 1$$

-Low magnetic Reynolds number,

$$Re_m = \sigma \mu L u_0 \ll 1$$





Challenges

Complex geometries

Balancing Lorentz force & pressure drop





Challenges

Complex geometries

→ Collocated grids

Balancing Lorentz force & pressure drop





Challenges

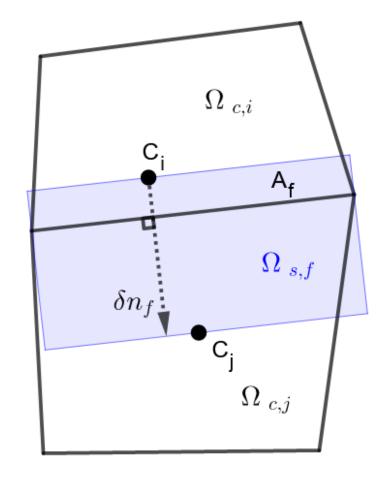
Complex geometries

→ Collocated grids

Balancing Lorentz force & pressure drop



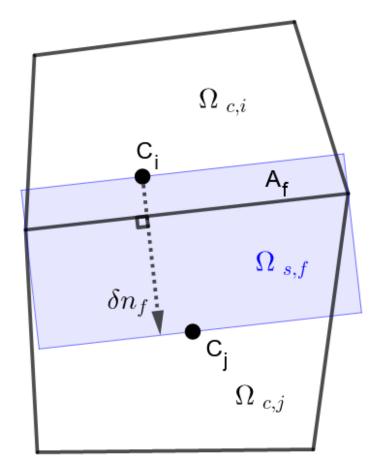








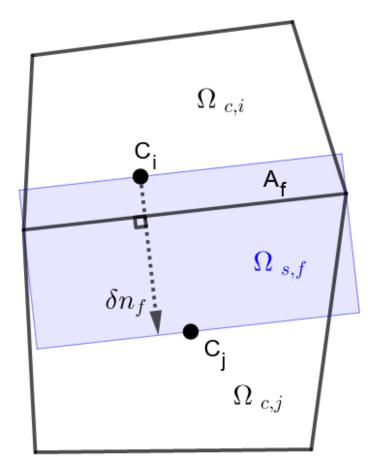
1. Projected gradient distances







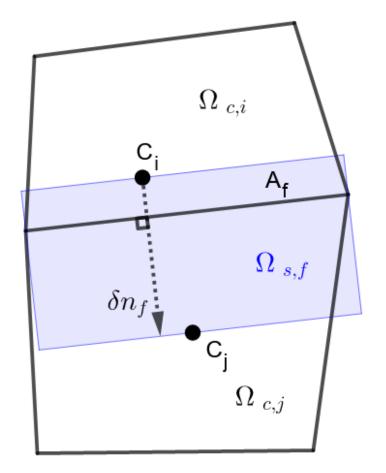
- 1. Projected gradient distances
- 2. Consistent Div, Grad, Lap







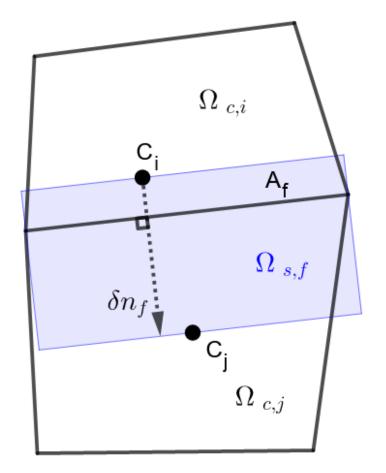
- 1. Projected gradient distances
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- 3. Midpoint interpolation in $C(\mathbf{u}_s)$







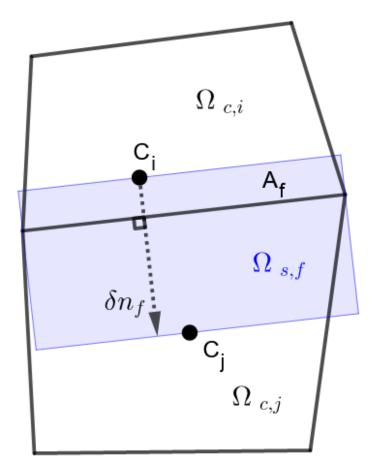
- 1. Projected gradient distances
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- 4. Volumetric interpolation







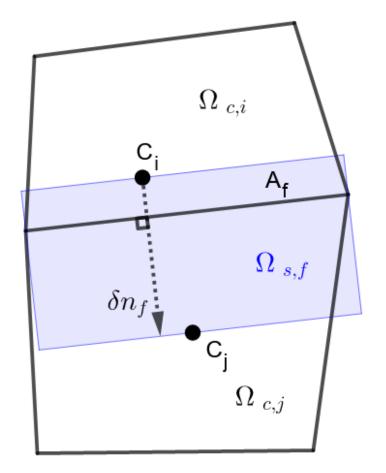
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 - Flux term of Poisson equation





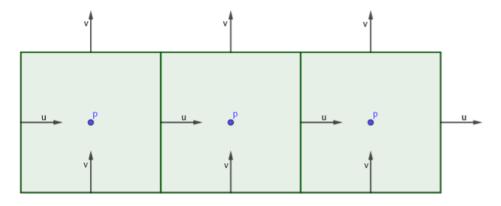


- 1. Projected gradient distances
- 2. Consistent Div, Grad, Lap
- 3. Midpoint interpolation in $C(\mathbf{u}_s)$
- 4. Volumetric interpolation
 - Flux term of Poisson equation
 - Correction term after Poisson



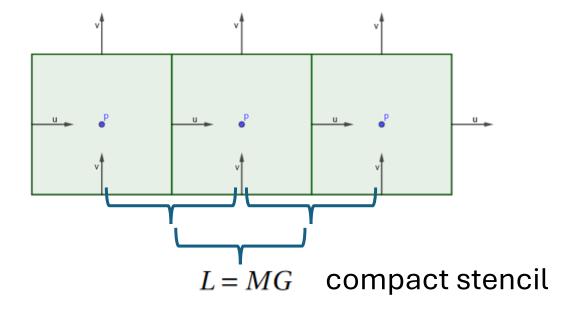


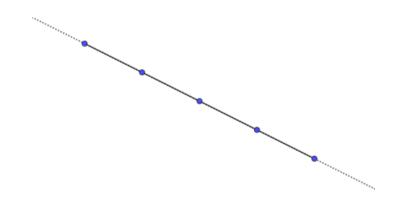






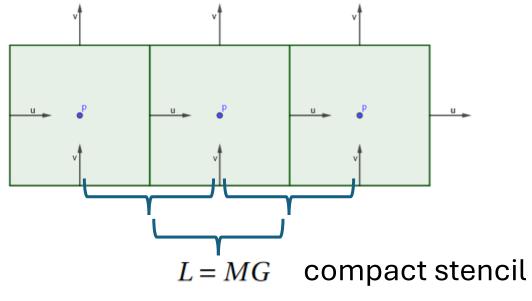


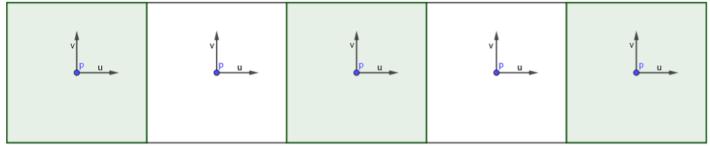


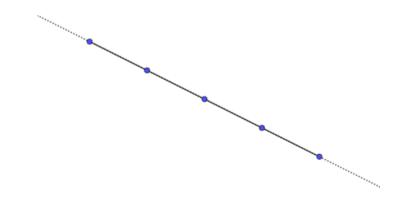






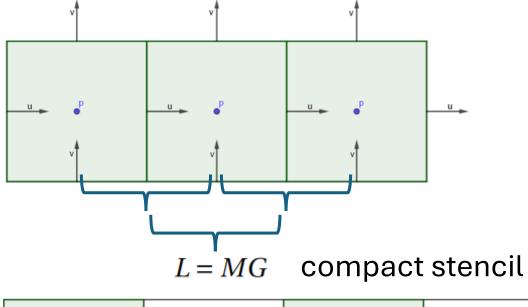


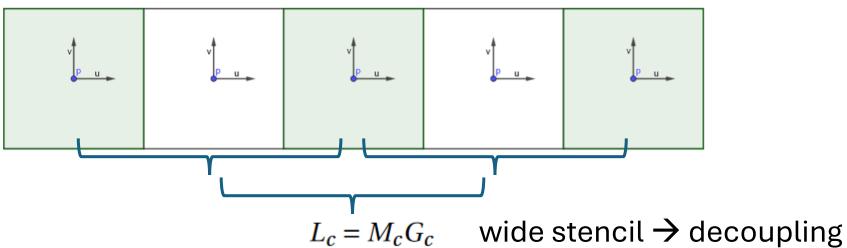


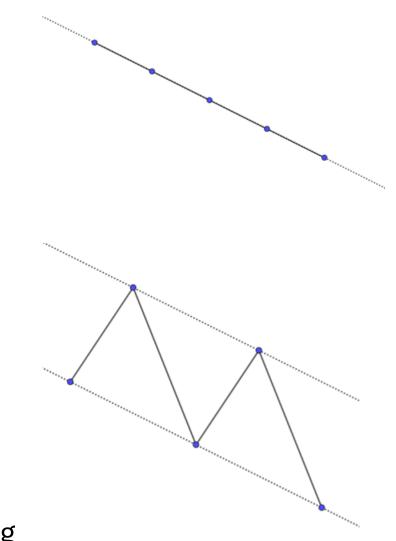






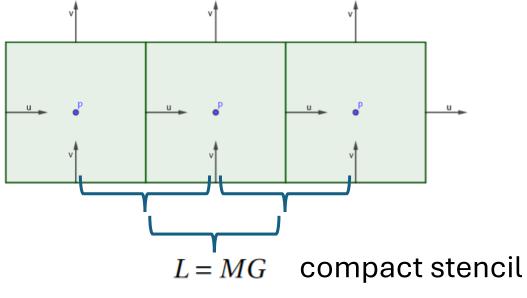


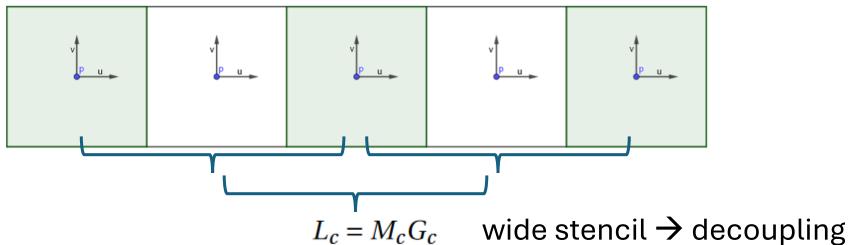


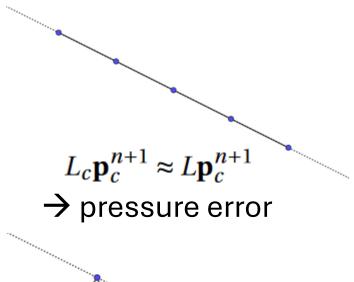
















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Lowering pressure error $\sim (L-L_c) \tilde{\mathbf{p}}_c'$

Larger part on $L_c \rightarrow More$ prone to checkerboarding





Induction-less approximation

Formulation of second Poisson equation

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = \nu \nabla^2 \mathbf{u} - \nabla (p/\rho) + (\mathbf{J} \times \mathbf{B}) / \rho, \qquad \nabla \cdot \mathbf{u} = 0,$$
$$\mathbf{J} = \sigma (-\nabla \phi + \mathbf{u} \times \mathbf{B}), \qquad \nabla \cdot \mathbf{J} = 0.$$





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$$\nabla^2 \phi = \nabla \cdot (\mathbf{u} \times \mathbf{B})$$









$$-\mathbf{u}_c^T \Omega G_c \mathbf{p}_c$$





$$-\mathbf{u}_c^T \Omega G_c \mathbf{p}_c = \mathbf{p}_c^T M_c \mathbf{u}_c$$





$$-\mathbf{u}_c^T \Omega G_c \mathbf{p}_c = \mathbf{p}_c^T M_c \mathbf{u}_c = \Delta t \mathbf{p}_c^T (L - L_c) \mathbf{p}_c$$





$$-\mathbf{u}_c^T \Omega G_c \mathbf{p}_c = \mathbf{p}_c^T M_c \mathbf{u}_c = \Delta t \mathbf{p}_c^T (L - L_c) \mathbf{p}_c \in [\Delta t \mathbf{p}_c^T L \mathbf{p}_c, 0]$$





Starting from the pressure budget term:

$$-\mathbf{u}_c^T \Omega G_c \mathbf{p}_c = \mathbf{p}_c^T M_c \mathbf{u}_c = \Delta t \mathbf{p}_c^T (L - L_c) \mathbf{p}_c \in [\Delta t \mathbf{p}_c^T L \mathbf{p}_c, 0]$$

$$C_{cb} = 1 - \frac{\mathbf{p}_c^T L_c \mathbf{p}_c}{\mathbf{p}_c^T L \mathbf{p}_c}$$





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Balance checkerboarding and accuracy

General predictor coefficient:

$$\theta_a = \frac{a_c^T L_c a_c}{a_c^T L a_c}$$





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General predictor coefficient:

$$\theta_a = \frac{a_c^T L_c a_c}{a_c^T L a_c}$$

Low Cb

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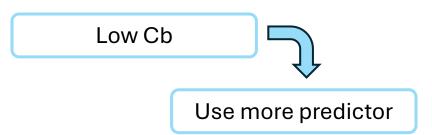




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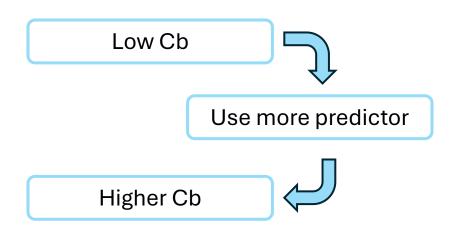




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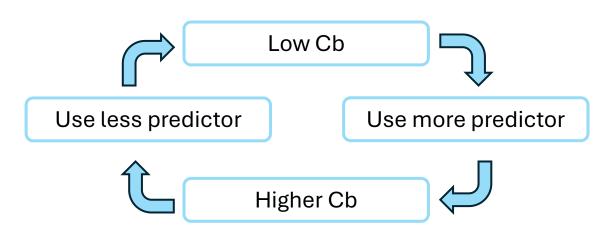




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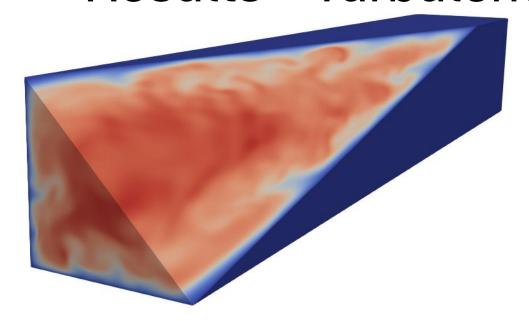
$$\theta_a = \frac{a_c^T L_c a_c}{a_c^T L a_c}$$

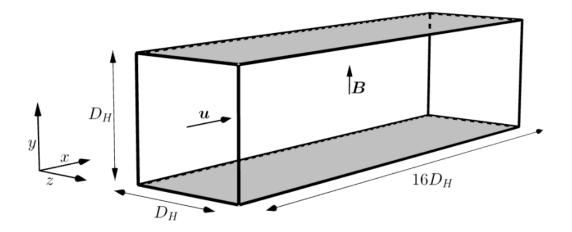
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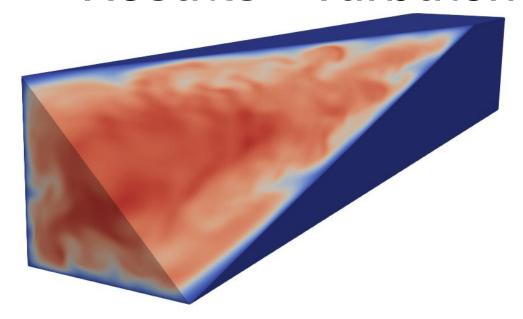


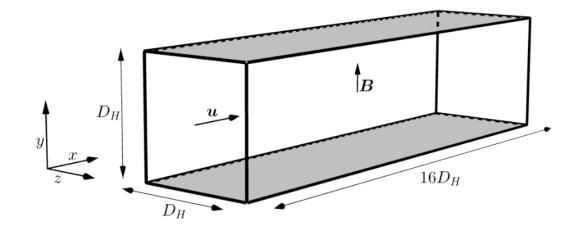








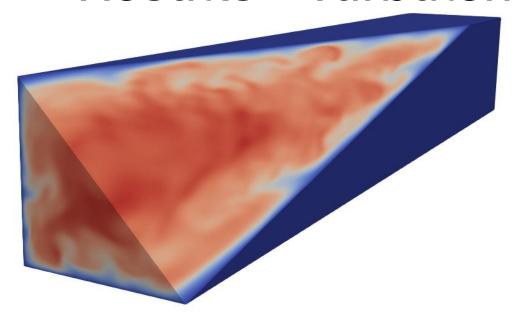


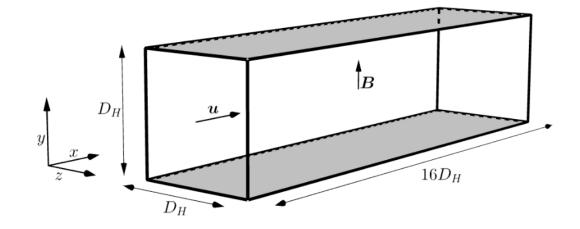


Hydrodynamic





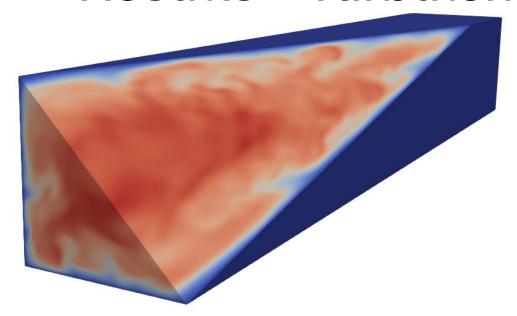




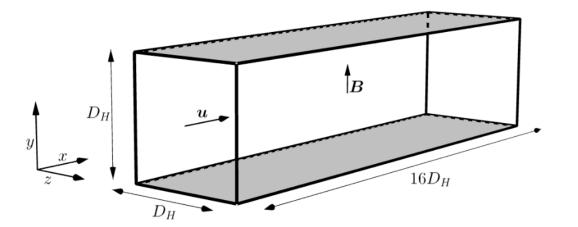
Hydrodynamic MHD





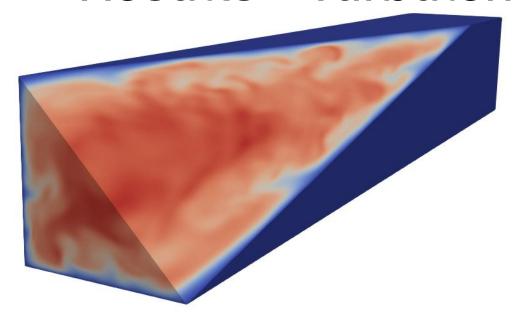


Hydrodynamic MHD Insulated (Shercliff)

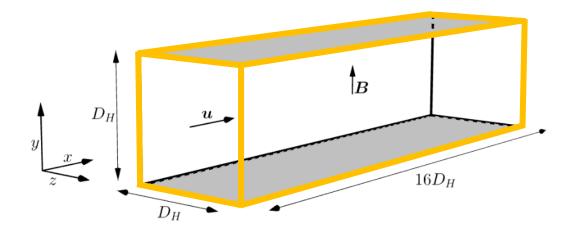






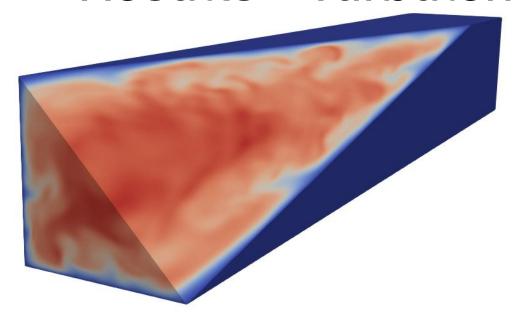


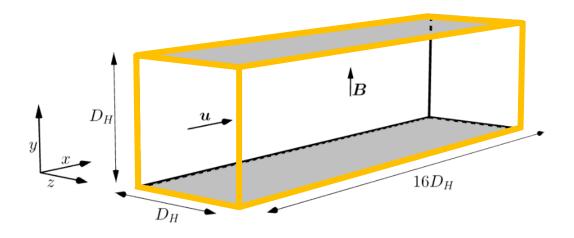
Hydrodynamic MHD Insulated (Shercliff) Conductive



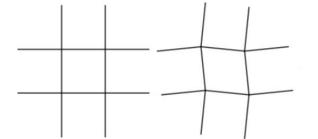






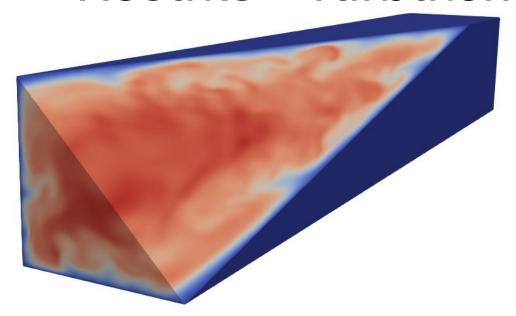


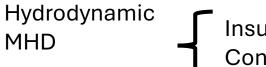
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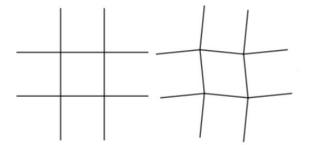


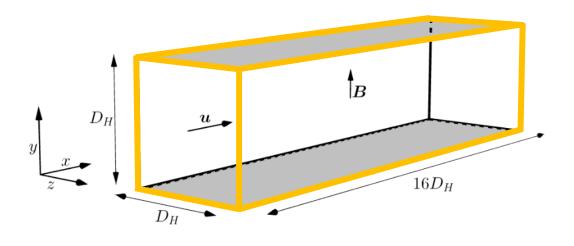






Insulated (Shercliff)
Conductive

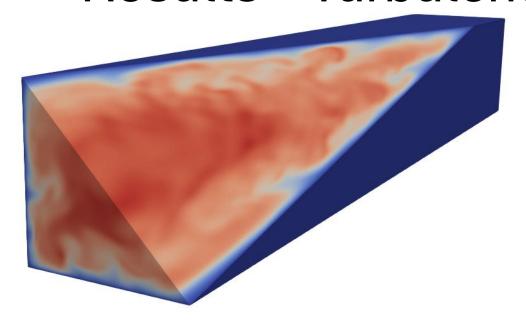




Mesh	L_x	N_x	$N_{\{y,z\}}$	$N_{tot}\left(\cdot 10^6 ight)$	Δx^+	$\Delta \{y,z\}_B^+$	$\Delta \{y,z\}_w^+$
H_{coarse}	$2\pi D_H$	160	64	0.66	11.8	9.1	0.9
H_{fine}	$2\pi D_H$	160	128	2.62	11.8	4.6	0.4
$\dot{M_{coarse}}$	$16D_H$	160	64	0.66	36.0	10.9	1.1
M_{fine}	$16D_H$	320	128	5.24	18.0	5.5	0.5

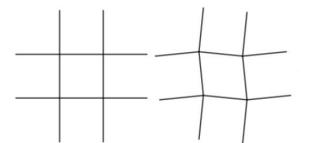


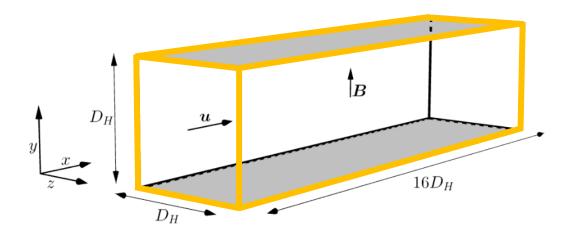




Hydrodynamic MHD

Insulated (Shercliff)
Conductive





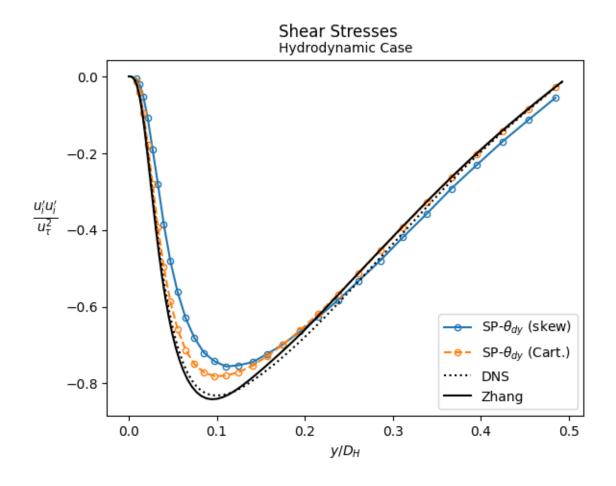
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$$\underbrace{\frac{1}{\rho}\overline{u_{i}'(\mathbf{J}\times\mathbf{B})_{i}'}}_{\text{Net MHD work}} = \underbrace{-\frac{\sigma}{\rho}\overline{u_{i}'((\nabla\phi)\times\mathbf{B})_{i}'}}_{M_{k}^{\phi}} + \underbrace{\frac{\sigma}{\rho}\overline{u_{i}'(\mathbf{u}\times\mathbf{B}\times\mathbf{B})_{i}'}}_{M_{k}^{u}}$$



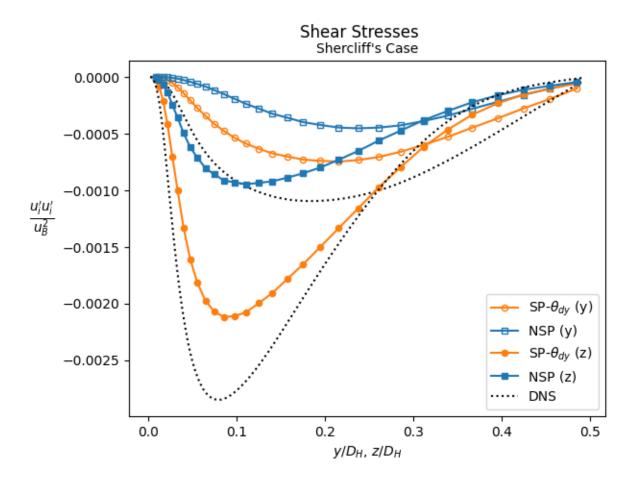


Results - Turbulent hydrodynamic duct flow



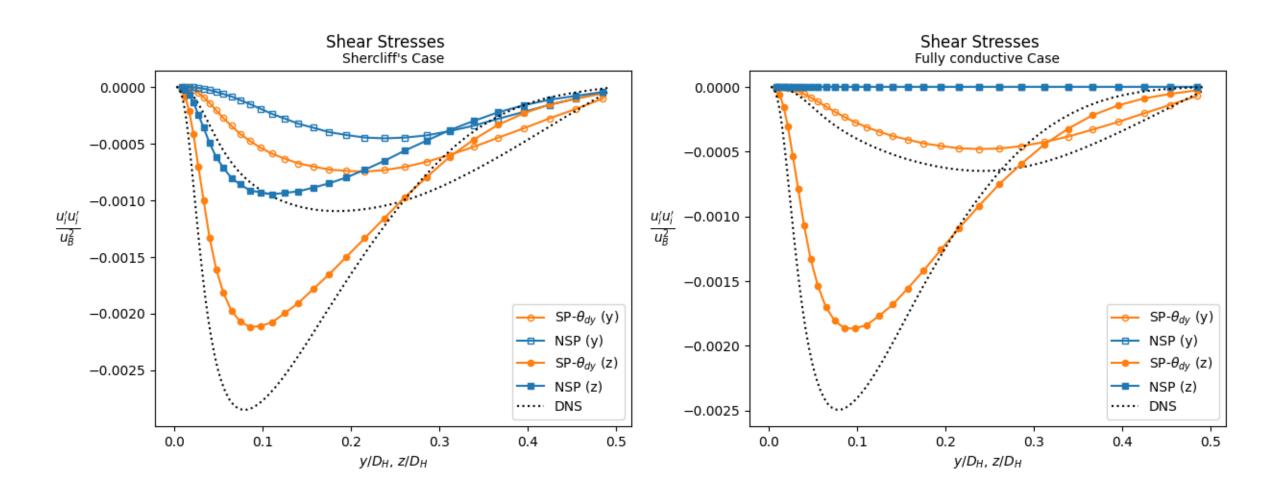






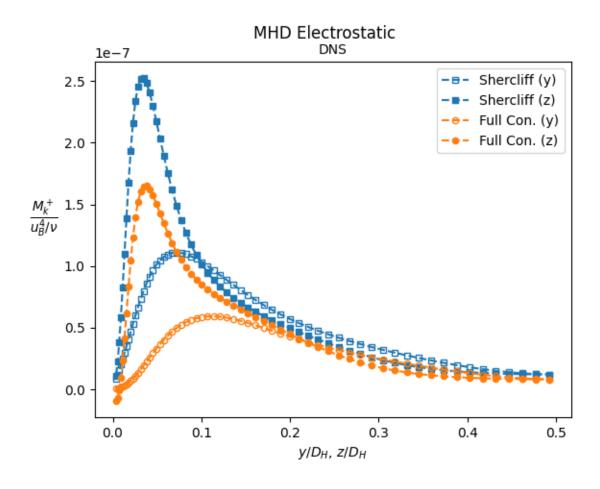






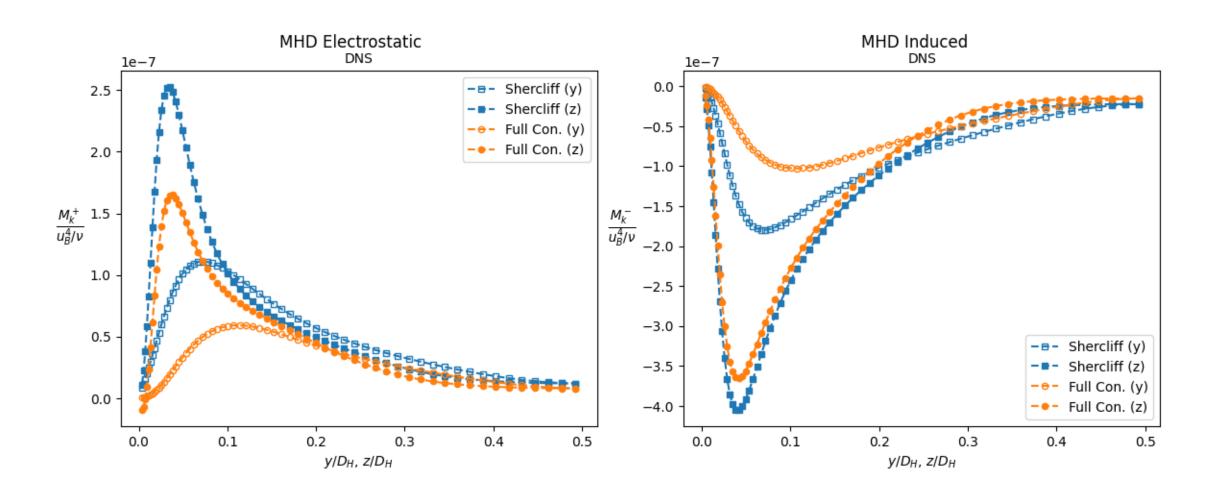
















				$\text{SP-}\theta_{dy}$			NSP			
Case	Mesh	Cells	p_{cb}	$\phi_{cb}\left(\cdot 10^{-3}\right)$	$Re_{\{ au/B\}}$	p_{cb}	$\phi_{cb}\left(\cdot 10^{-3}\right)$	$Re_{\{ au/B\}}$		
Hydrodyn.	H_{fine}	Cart.	0.14	0	4314[B]	-	-	-		
"	H_{coarse}	Cart.	0.32	0	4536[B]	0.37	0	4389[B]		
"	H_{coarse}	skew.	0.49	0	4787[B]	0.80	0	4826[B]		
Shercliff	M_{fine}	Cart.	0.13	0.17	$368.4[\tau]$	-	-	-		
"	$\dot{M_{coarse}}$	\mathbf{skew}	0.50	0.64	$351.7[\tau]$	0.89	0.61	$328.8[\tau]$		
Full Con.	M_{fine}	Cart.	0.12	2.75	$364.3[\tau]$	-	-	-		
"	M_{coarse}	\mathbf{skew}	0.49	8.33	$351.2[\tau]$	0.87	3.62	$317.9[\tau]$		





				$\text{SP-}\theta_{dy}$			NSP			
Case	Mesh	Cells	p_{cb}	$\phi_{cb}\left(\cdot 10^{-3}\right)$	$Re_{\{ au/B\}}$	p_{cb}	$\phi_{cb}\left(\cdot 10^{-3} ight)$	$Re_{\{ au/B\}}$		
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"	M_{coarse}	skew	0.50	0.64	$351.7[\tau]$	0.89	0.61	$328.8[\tau]$		
Full Con.	M_{fine}	Cart.	0.12	2.75	$364.3[\tau]$	-	-	-		
"	M_{coarse}	skew	0.49	8.33	$351.2[\tau]$	0.87	3.62	$317.9[\tau]$		









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- -Symmetry preserving method provides stability