



Centre Tecnològic de Transferència de Calor
UNIVERSITAT POLITÈCNICA DE CATALUNYA



On a proper tensorial subgrid heat flux model for LES

F.Xavier Trias¹, Andrey Gorobets², Assensi Oliva¹

¹Heat and Mass Transfer Technological Center, Technical University of Catalonia

²Keldysh Institute of Applied Mathematics of RAS, Russia

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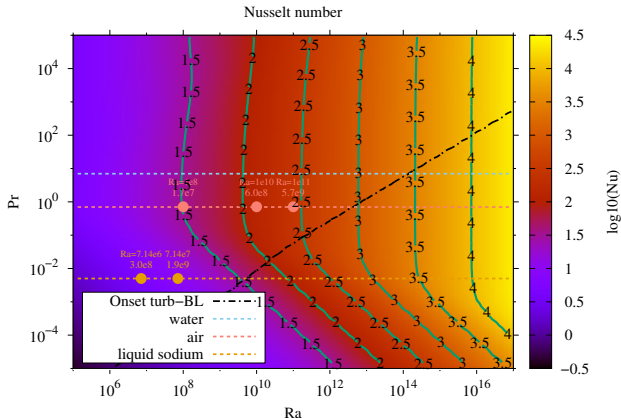
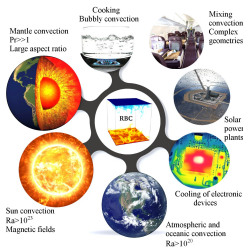
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Motivation

General research question:

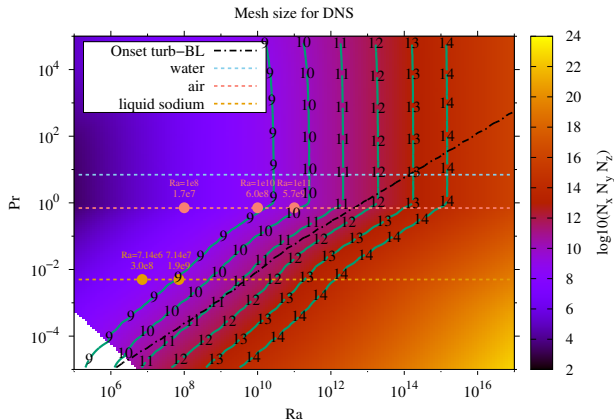
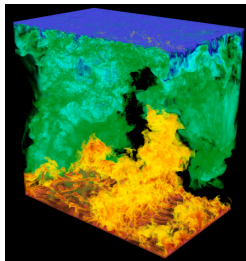
- Can we hit the ultimate regime of thermal turbulence ?



Motivation

General research question:

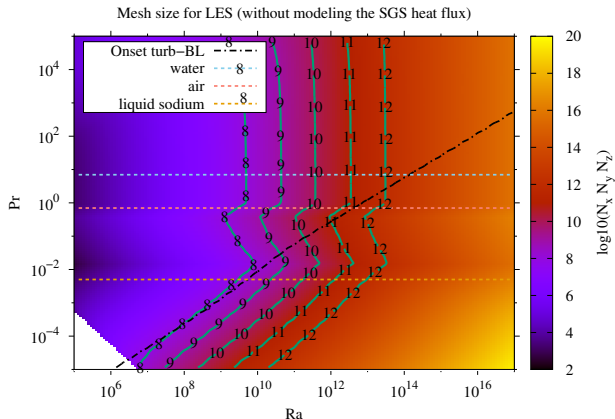
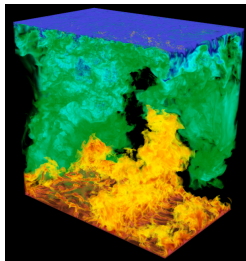
- Can we hit the ultimate regime of thermal turbulence with **DNS**?



Motivation

General research question:

- Can we hit the ultimate regime of thermal turbulence with **LES**?



How to model the subgrid heat flux in LES?

$$\partial_t \bar{\mathbf{u}} + (\bar{\mathbf{u}} \cdot \nabla) \bar{\mathbf{u}} = \nu \nabla^2 \bar{\mathbf{u}} - \nabla \bar{p} - \nabla \cdot \boldsymbol{\tau}(\bar{\mathbf{u}}) ; \quad \nabla \cdot \bar{\mathbf{u}} = 0$$

$$\text{eddy-viscosity} \longrightarrow \boldsymbol{\tau}(\bar{\mathbf{u}}) = -2\nu_t \mathbf{S}(\bar{\mathbf{u}})$$

$$\boxed{\nu_t \approx (C_m \delta)^2 D_m(\bar{\mathbf{u}})} \longrightarrow \{\text{WALE, Vreman, QR, Sigma, S3PQR, ...}\}$$

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$$G \equiv \nabla \bar{\mathbf{u}} \quad \mathbf{q} = -\frac{\delta^2}{12} G \nabla \bar{T} + \mathcal{O}(\delta^4)$$

A priori alignment trends¹

$$\text{eddy-diffusivity} \longrightarrow \mathbf{q} \approx -\alpha_t \nabla \bar{T} \quad (\equiv \mathbf{q}^{\text{eddy}})$$

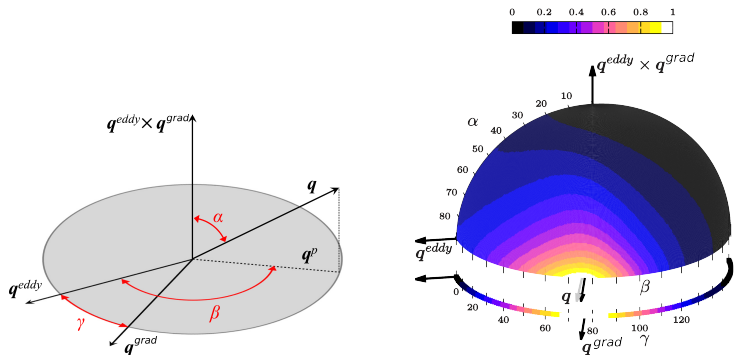
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¹F.Dabbagh, F.X.Trias, A.Gorobets, A.Oliva. *A priori study of subgrid-scale features in turbulent Rayleigh-Bénard convection*, **Physics of Fluids**, 29:105103, 2017.

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²S.Peng and L.Davidson. *Int.J.Heat Mass Transfer*, 45:1393-1405, 2002.

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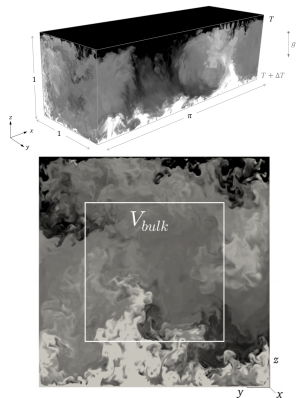
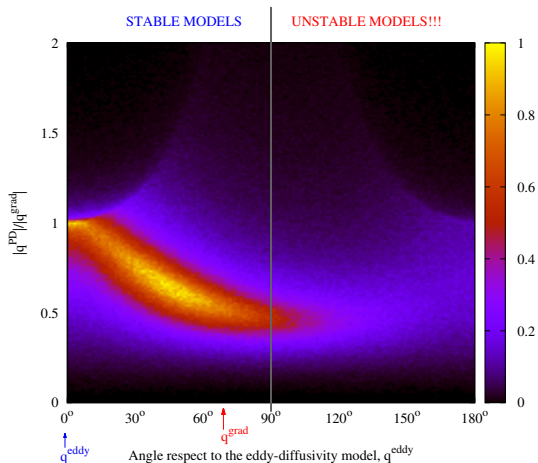
Peng&Davidson² $\rightarrow \mathbf{q} \approx -\frac{\delta^2}{12} S \nabla \bar{T} \quad (\equiv \mathbf{q}^{PD})$

²S.Peng and L.Davidson. *Int.J.Heat Mass Transfer*, 45:1393-1405, 2002.

A priori alignment trends

$$\mathbf{q}^{\text{grad}} \equiv -\frac{\delta^2}{12} G \nabla \bar{T}$$

$$\mathbf{q}^{\text{PD}} \equiv -\frac{\delta^2}{12} S \nabla \bar{T}$$



How to model the subgrid heat flux in LES?

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Deconstructing the gradient model

Research question #1:

- Can we implement the gradient model **re-using discrete operators** in such a way that we **avoid unnecessary interpolations**?

$$\text{gradient model} \longrightarrow \mathbf{q} \approx -\frac{\delta^2}{12} \nabla \bar{\mathbf{u}} \nabla \bar{T} \quad (\equiv \mathbf{q}^{grad})$$

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Continuous

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{C}(\mathbf{u}, \mathbf{u}) = \nu \nabla^2 \mathbf{u} - \nabla p$$

$$\nabla \cdot \mathbf{u} = 0$$

Discrete

$$\Omega \frac{d\mathbf{u}_h}{dt} + \mathbf{C}(\mathbf{u}_h) \mathbf{u}_h = \mathbf{D} \mathbf{u}_h - \mathbf{G} \mathbf{p}_h$$

$$\mathbf{M} \mathbf{u}_h = \mathbf{0}_h$$

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$$\nabla \cdot \mathbf{u} = 0$$

$$\langle \mathbf{C}(\mathbf{u}, \varphi_1), \varphi_2 \rangle = -\langle \mathbf{C}(\mathbf{u}, \varphi_2), \varphi_1 \rangle$$

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Discrete

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Discrete

$$\Omega \frac{d\mathbf{u}_h}{dt} + \mathbf{C}(\mathbf{u}_h) \mathbf{u}_h = \mathbf{D} \mathbf{u}_h - \mathbf{G} \mathbf{p}_h$$

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$$\Omega \mathbf{G} = -\mathbf{M}^T$$

$$\mathbf{D} = \mathbf{D}^T \quad \text{def -}$$

Deconstructing the gradient model

Continuous

$$\mathbf{q}^{grad} = -\frac{\delta^2}{12} \nabla \mathbf{u} \nabla T$$

Discrete

????

Deconstructing the gradient model

Continuous

$$\mathbf{q}^{grad} = -\frac{\delta^2}{12} \nabla \mathbf{u} \nabla T$$

$$-\nabla \cdot \mathbf{q}^{grad} =$$

Discrete

????

Deconstructing the gradient model

Continuous

$$\mathbf{q}^{grad} = -\frac{\delta^2}{12} \nabla \mathbf{u} \nabla T$$

$$-\nabla \cdot \mathbf{q}^{grad} =$$

Discrete

????

$$C(\mathbf{u}, T) - \widetilde{C(\mathbf{u}, T)} = \frac{\tilde{\delta}^2}{24} \nabla^2 \nabla \cdot (\mathbf{u} T) = \frac{\tilde{\delta}^2}{24} \nabla \cdot \nabla^2 (\mathbf{u} T)$$

$$C(\mathbf{u}, T) - C(\tilde{\mathbf{u}}, T) = \frac{\tilde{\delta}^2}{24} \nabla \cdot ((\nabla^2 \mathbf{u}) T)$$

$$C(\mathbf{u}, T) - C(\mathbf{u}, \tilde{T}) = \frac{\tilde{\delta}^2}{24} \nabla \cdot (\mathbf{u} \nabla^2 T)$$

Deconstructing the gradient model

Continuous

$$\mathbf{q}^{grad} = -\frac{\delta^2}{12} \nabla \mathbf{u} \nabla T$$

$$-\nabla \cdot \mathbf{q}^{grad} = C(\mathbf{u}, T) + \widetilde{C(\mathbf{u}, T)}$$

$$- C(\tilde{\mathbf{u}}, T) - C(\mathbf{u}, \tilde{T})$$

Discrete

????

$$C(\mathbf{u}, T) - \widetilde{C(\mathbf{u}, T)} = \frac{\tilde{\delta}^2}{24} \nabla^2 \nabla \cdot (\mathbf{u} T) = \frac{\tilde{\delta}^2}{24} \nabla \cdot \nabla^2 (\mathbf{u} T)$$

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Deconstructing the gradient model

Continuous

$$\mathbf{q}^{grad} = -\frac{\delta^2}{12} \nabla \mathbf{u} \nabla T$$

$$-\nabla \cdot \mathbf{q}^{grad} = C(\mathbf{u}, T) + \widetilde{C(\mathbf{u}, T)} \\ - C(\tilde{\mathbf{u}}, T) - C(\mathbf{u}, \tilde{T})$$

Discrete

????

$$-\mathbf{M} \mathbf{q}_h^{grad} = C(\mathbf{u}_h) T_h + \mathbf{F} C(\mathbf{u}_h) T_h \\ - C(\mathbf{F} \mathbf{u}_h) T_h - C(\mathbf{u}_h) \mathbf{F} T_h$$

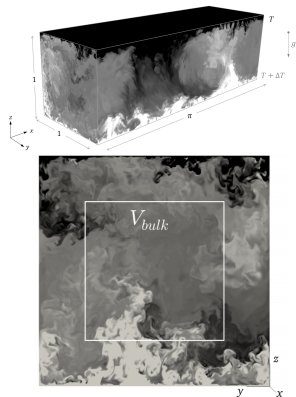
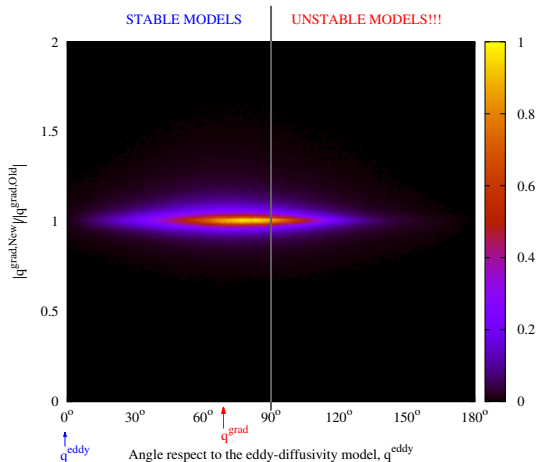
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$$C(\mathbf{u}, T) - C(\mathbf{u}, \tilde{T}) = \frac{\tilde{\delta}^2}{24} \nabla \cdot (\mathbf{u} \nabla^2 T)$$

Deconstructing the gradient model

$$-M \mathbf{q}_h^{grad} = C(\mathbf{u}_h) T_h + FC(\mathbf{u}_h) T_h - C(F\mathbf{u}_h) T_h - C(\mathbf{u}_h) F T_h$$



Deconstructing the gradient model

$$-M\mathbf{q}_h^{grad} = C(\mathbf{u}_h)T_h + FC(\mathbf{u}_h)T_h - C(F\mathbf{u}_h)T_h - C(\mathbf{u}_h)FT_h$$

Deconstructing the gradient model

$$-M\mathbf{q}_h^{grad} = \mathbf{C}(\mathbf{u}_h)T_h + \mathbf{F}\mathbf{C}(\mathbf{u}_h)T_h - \mathbf{C}(\mathbf{F}\mathbf{u}_h)T_h - \mathbf{C}(\mathbf{u}_h)\mathbf{F}T_h$$

$$-M\mathbf{q}_h^{grad} = \begin{pmatrix} \mathbf{I} \\ \mathbf{F} \end{pmatrix}^T \begin{pmatrix} \mathbf{C}(\mathbf{u}_h) - \mathbf{C}(\mathbf{F}\mathbf{u}_h) & \boxed{-\mathbf{C}(\mathbf{u}_h)} \\ \boxed{\mathbf{C}(\mathbf{u}_h)} & 0 \end{pmatrix} \begin{pmatrix} \mathbf{I} \\ \mathbf{F} \end{pmatrix} T_h$$

Deconstructing the gradient model

$$-M\mathbf{q}_h^{grad} = C(\mathbf{u}_h)T_h - RC(\mathbf{u}_h)T_h - C(F\mathbf{u}_h)T_h + C(\mathbf{u}_h)RT_h$$

$$-M\mathbf{q}_h^{grad} = \begin{pmatrix} I \\ F \end{pmatrix}^T \begin{pmatrix} C(\mathbf{u}_h) - C(F\mathbf{u}_h) & \boxed{-C(\mathbf{u}_h)} \\ \boxed{C(\mathbf{u}_h)} & 0 \end{pmatrix} \begin{pmatrix} I \\ F \end{pmatrix} T_h$$

Alternatively, it can be expressed as follows

$$-M\mathbf{q}_h^{grad} = \begin{pmatrix} I \\ R \end{pmatrix}^T \begin{pmatrix} C(\mathbf{u}_h) - C(F\mathbf{u}_h) & \boxed{C(\mathbf{u}_h)} \\ \boxed{-C(\mathbf{u}_h)} & 0 \end{pmatrix} \begin{pmatrix} I \\ R \end{pmatrix} T_h$$

where $F = I - R$.

Deconstructing the gradient model

$$-M\mathbf{q}_h^{grad} = C(\mathbf{u}_h)T_h - RC(\mathbf{u}_h)T_h - C(F\mathbf{u}_h)T_h + C(\mathbf{u}_h)RT_h$$

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where $F = I - R$. Recalling that $C = -C^T$ and $F = F^T$, leads to

$$-T_h \cdot M\mathbf{q}_h^{grad} = T_h \cdot (RC - CR)T_h$$

Deconstructing the gradient model

$$-M\mathbf{q}_h^{grad} = C(\mathbf{u}_h)T_h - RC(\mathbf{u}_h)T_h - C(F\mathbf{u}_h)T_h + C(\mathbf{u}_h)RT_h$$

Stability is determined by the sign of the Rayleigh quotient of $RC - CR$

$$-M\mathbf{q}_h^{grad} = \begin{pmatrix} I \\ F \end{pmatrix}^T \begin{pmatrix} C(\mathbf{u}_h) - C(F\mathbf{u}_h) & \boxed{-C(\mathbf{u}_h)} \\ \boxed{C(\mathbf{u}_h)} & 0 \end{pmatrix} \begin{pmatrix} I \\ F \end{pmatrix} T_h$$

Alternatively, it can be expressed as follows

$$-M\mathbf{q}_h^{grad} = \begin{pmatrix} I \\ R \end{pmatrix}^T \begin{pmatrix} C(\mathbf{u}_h) - C(F\mathbf{u}_h) & \boxed{C(\mathbf{u}_h)} \\ \boxed{-C(\mathbf{u}_h)} & 0 \end{pmatrix} \begin{pmatrix} I \\ R \end{pmatrix} T_h$$

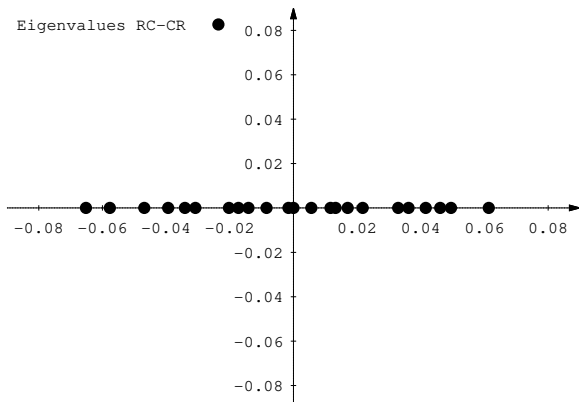
where $F = I - R$. Recalling that $C = -C^T$ and $F = F^T$, leads to

$$-T_h \cdot M\mathbf{q}_h^{grad} = T_h \cdot (RC - CR)T_h$$

Stabilizing the gradient model

$$-M \mathbf{q}_h^{grad} = C(\mathbf{u}_h) T_h - RC (\mathbf{u}_h) T_h - C(F\mathbf{u}_h) T_h + C(\mathbf{u}_h) R T_h$$

Stability is determined by the sign of the Rayleigh quotient of $RC - CR$

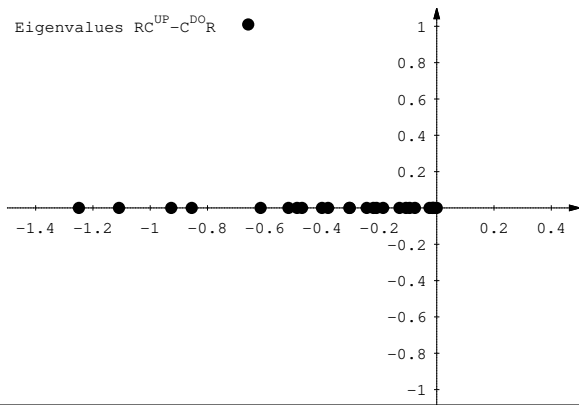


$RC - CR$

Stabilizing the gradient model

$$-M \mathbf{q}_h^{grad} = C(\mathbf{u}_h) T_h - RC^{UP}(\mathbf{u}_h) T_h - C(F\mathbf{u}_h) T_h + C^{DO}(\mathbf{u}_h) R T_h$$

Stability is determined by the sign of the Rayleigh quotient of $RC - CR$



Idea: $RC^{UP} - C^{DO}R$ instead of $RC - CR$ guarantees stability

Stabilizing the gradient model

Test-case: passive scalar in a 2D channel flow

Stabilizing the gradient model

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Stabilizing the gradient model

Test-case: passive scalar in a 2D channel flow

$$-M \mathbf{q}_h^{grad} = C(\mathbf{u}_h) T_h \boxed{-RC} (\mathbf{u}_h) T_h - C(F\mathbf{u}_h) T_h \boxed{+C} (\mathbf{u}_h) R T_h$$

Stabilizing the gradient model

Test-case: passive scalar in a 2D channel flow

$$-\mathbf{M}\mathbf{q}_h^{grad} = C(\mathbf{u}_h)T_h \boxed{-\mathbf{R}C^{UP}(\mathbf{u}_h)T_h} - C(\mathbf{F}\mathbf{u}_h)T_h \boxed{+C^{DO}(\mathbf{u}_h)\mathbf{R}T_h}$$

Concluding remarks

- A new way to implement the gradient model has been proposed ✓

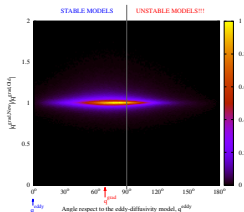
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- Good *a priori* alignment trends ✓



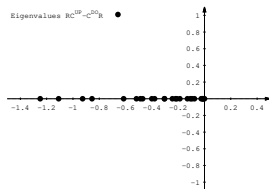
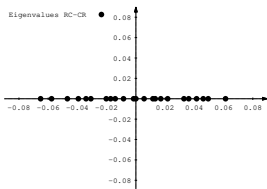
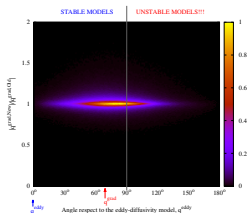
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- Good *a priori* alignment trends ✓
- Stabilization has been proposed and tested ✓

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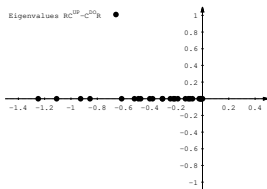
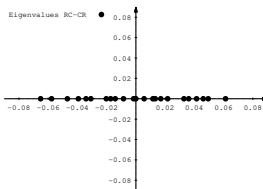
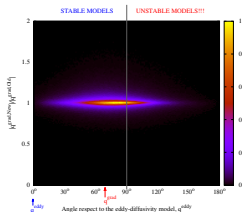
Concluding remarks

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$$-Mq_h^{grad} = C(u_h)T_h - RC(u_h)T_h - C(Fu_h)T_h + C(u_h)RT_h$$

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$$-Mq_h^{grad} = C(u_h)T_h - RC^{UP}(u_h)T_h - C(Fu_h)T_h + C^{DO}(u_h)RT_h$$



- On going research: running *a posteriori* for more complex cases

Thank you for your attendance