Introduction	Mathematical Machinery	Flux Limiters	Results	Conclusions

Algebraic implementation of a flux limiter for heterogeneous computing

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July 16, 2018

10th International Conference in Computational Fluid Dynamics July, 9-13, 2018, Barcelona

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Overview				



- Motivation
- Inspiration
- 2 Mathematical Machinery
 - Algebraic Topology
 - Mimetic/Symmetry preserving schemes
- 3 Flux Limiters
 - High Resolution Schemes
 - Gradient Ratio
 - Implementation
- 4 Results
 - Periodic Advection



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Portability.	Why?			

Software

- Legacy codes
- Architecture-dependent
- Non-standard kernels

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Portability.	Why?			

Software

- Legacy codes
- Architecture-dependent
- Non-standard kernels

Hardware

- New architectures
- Hybrid platforms
- Power consumption

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Portability.	Why?			

Software

- Legacy codes
- Architecture-dependent
- Non-standard kernels

Hardware

- New architectures
- Hybrid platforms
- Power consumption

Challenge

How to design portable/hybrid platform codes?

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Portability.	How?			
Idea				

Mathematics are always portable!

Portability.	How?			
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Idea

Mathematics are always portable!

"The reason MATLAB is so good at signal processing is that it was not designed for signal processing. It was designed to do mathematics."

> Jim McClellan GeorgiaTech

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Portability.	How?			

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> Jim McClellan GeorgiaTech

May approaching dedicated scientific computing codes from an algebraic perspective help?

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Portability.	What for?			

Casting **computational** operations into **algebraic** forms provides with several advantages:

- fewer number of computing kernels \rightarrow portability
- $\bullet\,$ mathematical formality $\rightarrow\,$ analysis

Remark¹

For a typical DNS simulation of an incompressible flow, almost 90% of the operations can be cast into 3 basic kernels:

- SpMV
- DOT
- axpy

¹Guillermo Oyarzun et al. "Portable implementation model for CFD simulations. Application to hybrid CPU/GPU supercomputers". In: *Int. J. Comut. Fluid Dyn.* 31.9 (2017), pp. 396–411.

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Scope				

How to design a flux limiter kernel from an algebraic approach?

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Advantages

With this approach we aim at:

- High portability
- High degree of abstraction

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How to design a flux limiter kernel from an algebraic approach?

Advantages

With this approach we aim at:

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Disclaimer

We are not after:

- Discussing Flux Limiters
- Optimize performance

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Algebraic T	opology			

Your mesh. A starting point.







Figure 2: Dual mesh

Algebraic T	opology			
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DeRahm Cohomology

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Algebraic	Topology			
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DeRahm Cohomology

Under the hood of:

- Staggered grid
- Symmetry preserving

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A graph	to rule them all			



$$T_{cf} = \begin{array}{c} f_1 & f_2 & f_3 & f_4 & f_5 & f_6 & f_7 & f_8 & f_9 \\ c_1 \\ c_2 \\ c_3 \\ c_4 \end{array} \begin{pmatrix} 0 & 0 & +1 & -1 & -1 & 0 & 0 & 0 & 0 \\ +1 & +1 & -1 & 0 & 0 & 0 & 0 & 0 & 0 \\ -1 & 0 & 0 & 0 & 0 & +1 & -1 & 0 & 0 \\ 0 & -1 & 0 & 0 & 0 & 0 & 0 & -1 & -1 \end{pmatrix}$$

Operators

Operators can be constructed from graph information.

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A graph t	o rule them all			

Example: Gradient operator

$$\int_{c_3}^{c_2} \nabla P = P_2 - P_3$$

$$T_{cf} = \begin{array}{c} f_1 & f_2 & f_3 & f_4 & f_5 & f_6 & f_7 & f_8 & f_9 \\ c_1 \\ c_2 \\ c_3 \\ c_4 \end{array} \begin{pmatrix} 0 & 0 & +1 & -1 & -1 & 0 & 0 & 0 & 0 \\ +1 & +1 & -1 & 0 & 0 & 0 & 0 & 0 & 0 \\ -1 & 0 & 0 & 0 & 0 & +1 & -1 & 0 & 0 \\ 0 & -1 & 0 & 0 & 0 & 0 & 0 & -1 & -1 \end{pmatrix}$$

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A graph to	rule them all			

Example: Divergence operator

$$\int_{c_2} \nabla \cdot \vec{u} = \int_{\partial c_2} \vec{u} \hat{n}_f \approx \sum_{f \in c_2} S_f u_f$$

$$T_{cf} = \begin{array}{c} f_1 & f_2 & f_3 & f_4 & f_5 & f_6 & f_7 & f_8 & f_9 \\ c_1 & \begin{pmatrix} 0 & 0 & +1 & -1 & -1 & 0 & 0 & 0 & 0 \\ +1 & +1 & -1 & 0 & 0 & 0 & 0 & 0 & 0 \\ -1 & 0 & 0 & 0 & 0 & +1 & -1 & 0 & 0 \\ 0 & -1 & 0 & 0 & 0 & 0 & 0 & -1 & -1 \end{pmatrix}$$

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Summary				

Metric

Development of numerical method in terms of geometric entities.

$$\Omega_f = \Delta_x S_f$$

Symmetry-preserving

$$GRAD = -\Omega_f^{-1}DIV^T = -(\Delta_x S_f)^{-1}(T_{cf}S_f)^T = -(\Delta_x)^{-1}T_{cf}^T$$

Highlights

- The definition of star (*) determines dual operators
- Preserve important quantities

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Typically, flux limiters are stated in the following form:

$$\theta_{f} = \theta_{C} + \Psi(r) \left(\frac{\theta_{D} - \theta_{U}}{2} \right)$$
$$r_{f} = \frac{\theta_{C} - \theta_{U}}{\theta_{D} - \theta_{C}} = \frac{\Delta_{U}\theta_{c}}{\Delta_{u}\theta_{c}}$$
$$\underbrace{\overrightarrow{U}}_{U} \underbrace{\overrightarrow{U}}_{C} \underbrace{\overrightarrow{U}}_{D} \underbrace{\overrightarrow{U}} \underbrace{\overrightarrow{U}}_{D} \underbrace{\overrightarrow{U}}_{D} \underbrace{\overrightarrow{U}}_{D} \underbrace{\overrightarrow{U}}_{D} \underbrace{\overrightarrow{U}}_{D}$$

i + 1/2

Figure 3: Classical stencil for the computation of the gradient ratio at face i + 1/2. *U*, *C* and *D* correspond to the upstream, centered and downstream nodes.

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Reformulation in terms of matrices ² Rearrangement:

$$heta_f = rac{ heta_D + heta_U}{2} + rac{\Psi(r) - 1}{2} \left(heta_D - heta_U
ight)$$

Matrix formulation:

$$\theta_f = \left(\prod_{C \to F} + F(r)_{C \to F} \right) \theta_c$$

Dynamic addition of artificial diffusivity as a function of r

²F.X. Trias et al. "Symmetry-preserving discretization of Navier-Stokes equations on collocated unstructured grids". In: *J. Comput. Phys.* 258 (Feb. 2014), pp. 246–267.

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Figure 4: Switched stencil for a typical flux limiter

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Figure 4: Switched stencil for a typical flux limiter



Figure 5: Algebraic stencil for an algebraic flux limiter

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Figure 4: Switched stencil for a typical flux limiter



$$r_f = \frac{\theta_C - \theta_U}{\theta_D - \theta_C} = \frac{\Delta_U \theta_c}{\Delta_u \theta_c}$$

Figure 5: Algebraic stencil for an algebraic flux limiter

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Figure 4: Switched stencil for a typical flux limiter



$$r_{f} = \frac{\theta_{C} - \theta_{U}}{\theta_{D} - \theta_{C}} = \frac{\Delta_{U}\theta_{c}}{\Delta_{u}\theta_{c}}$$
$$\Delta_{u} = S(u)T_{cf}\theta_{c}$$

Figure 5: Algebraic stencil for an algebraic flux limiter

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Figure 4: Switched stencil for a typical flux limiter



Figure 5: Algebraic stencil for an algebraic flux limiter

$$r_f = \frac{\theta_C - \theta_U}{\theta_D - \theta_C} = \frac{\Delta_U \theta_c}{\Delta_u \theta_c}$$

$$\Delta_u = S(u) T_{cf} \theta_c$$

How to compute Δ_U ?

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Computing Δ_U



Figure 6: Upstream and Downstream adjacency faces $z \rightarrow z \rightarrow z$

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Idea

- Vectorize differences
- ② Sum up upstream faces
- Project over the normal



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Gradient R	atio			

Idea

- Vectorize differences
- ② Sum up upstream faces
- Project over the normal

$$\Delta_U = N\left(\mathbb{I}_d \otimes A^U_{FF(u)}\right) N^T \Delta$$





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Idea Vectoriz Sum up Project $\Delta_U = N \left(\begin{pmatrix} n_{1x} & 0 \\ \vdots & 0 \\ 0 & 0 \end{pmatrix} \right)$ $A_{FF(u)}^U = \frac{1}{2}$	e differences upstream faces over the normal $\mathbb{I}_{d} \otimes A_{FF(u)}^{U} N^{T} \Delta$ $\mathbb{O} \qquad 0 \qquad n_{1y} \qquad 0$ $\mathbb{O} \qquad \mathbb{O} \qquad $	\hat{n}_{5} \hat{v}_{2} \hat{n}_{4} \hat{v}_{1} \hat{v}_{1}	v_3 \hat{n}_1 \hat{n}_2 \hat{n}_2 \hat{n}_2 \hat{n}_2 \hat{n}_3 \hat{n}_4 \hat{n}_5 \hat{n}_6 \hat{n}	n ₇ n ⁷ n ⁷

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Idea Vectoriz Sum up Project $\Delta_U = N \left(\begin{pmatrix} n_{1x} & 0 \\ \vdots & 0 \\ 0 & 0 \end{pmatrix} \right)$ $A_{FF(u)}^U = \frac{1}{2}$	e differences upstream faces over the normal $\mathbb{I}_{d} \otimes A_{FF(u)}^{U} N^{T} \Delta$ $\mathbb{O} \qquad 0 \qquad n_{1y} \qquad 0 \\ \therefore \qquad \vdots \qquad \vdots \qquad \ddots \qquad \vdots \\ \mathbb{O} \qquad n_{9x} \qquad 0 \qquad \dots \qquad n_{9y} N^{T} \Delta$		v_3 \dot{n} \dot{n} \dot{n}	¢ v4 n7 n7 17/22

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Idea Vectoriz Sum up Project $\Delta_U = N \left(\begin{pmatrix} n_{1x} & 0 \\ \vdots & 0 \\ 0 & 0 \end{pmatrix} \right)$ $A_{FF(u)}^U = \frac{1}{2}$	e differences upstream faces over the normal $\mathbb{I}_{d} \otimes A_{FF(u)}^{U} N^{T} \Delta$ $\mathbb{O} \qquad 0 \qquad n_{1y} \qquad 0^{Y}$ $\mathbb{O} \qquad 0 \qquad n_{1y} \qquad 0^{Y}$ $\mathbb{O} \qquad 0 \qquad n_{1y} \qquad 0^{Y}$ $\mathbb{O} \qquad 0 \qquad n_{9x} \qquad 0 \qquad \dots \qquad n_{9y}$ $\left(S(u)A_{FF} - A_{FF}^{D}\right)$		v_3 \hat{n} \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot	6 n̂ ₇ n̂ ₇ 17/22

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Idea Vectoriz Sum up Project $\Delta_U = N \left(\begin{pmatrix} n_{1x} & 0 \\ \vdots & 0 \\ 0 & 0 \end{pmatrix} \right)$ $A_{FF(u)}^U = \frac{1}{2}$	e differences upstream faces over the normal $\mathbb{I}_{d} \otimes A_{FF(u)}^{U} N^{T} \Delta$ $\mathbb{O} \qquad 0 \qquad n_{1y} \qquad 0$ $\mathbb{O} \qquad \mathbb{O} \qquad $	\hat{n}_{5} \hat{v}_{2} \hat{n}_{4} \hat{v}_{1} \hat{v}_{1}	v_3 \hat{n}_1 \hat{n}_2 \hat{n}_2 \hat{n}_2 \hat{n}_2 \hat{n}_3 \hat{n}_4 \hat{n}_5 \hat{n}_6 \hat{n}	\hat{n}_7

Computatio	nal framework			
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The code has been implemented into HPC^2 - a fully-portable, algebra-based framework for heterogeneous computing ³.

Operation	SpMV	axpy	axdy	shft	scal	vmax	smax	sign
						vmin	smin	
S(u)	0	0	0	0	0	0	0	1
$\Delta_U \theta$	3	1	0	0	0	0	0	0
$\Delta_u \theta$	2	0	0	0	0	0	0	0
r _f	0	0	1	0	0	0	0	0
SUPERBEE(r)	0	0	0	1	1	1	3	0
$F(r)_{C \to F}$	0	0	0	0	1	0	0	0
Euler	6	2	0	0	0	0	0	0
total	11	3	1	1	2	1	3	1

Table 1: Operation count per time step with SUPERBEE and Euler integration ⁴.

³X Álvarez et al. "HPC² - a fully-portable, algebra-based framework for heterogeneous computing. Application to CFD". . In: *Comput. Fluids (published online)* (2018).

⁴X Álvarez et al. "Integration of a flux limiter into a fully-portable, algebra-based framework for heterogeneous computing". In: *Tenth Int. Conf. Comput. Fluid Dyn.* Barcelona, 2018.

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Advection of a scalar field					

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Drafiles				





Figure 7: Left column corresponds to a meshes with a characteristic length of $\Delta x = 1/32$, while right columns are produced with a characteristic length of $\Delta x = 1/64$.

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Highlights

- Flux limiters have been implemented into a portable platform
- Flux limiters CAN be cast in an algebraic form
- New conceptual platform developed

Future Work

- Analyze flux limiters properties
- Assess flux limiters design
- Improve gradient reconstruction strategies

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Thank you for your attention!