

Preserving symmetries on unstructured grids

F.Xavier Trias



Preserving symmetries on unstructured grids: paving the way for DNS and LES on complex geometries

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About myself...

Professional...

- Current position (since 2018): Associate Professor at UPC
- Previous positions: PostDoc at University of Groningen (2007-2009) and UPC (2010-2013), and Ramón y Cajal Senior Researcher at UPC (2013-2018).
- My research focus is on fluid mechanics, turbulence modeling, physics and numerics of complex flows, applied mathematics and numerical methods.
- Some numbers: 48 papers, 125 conferences, 7 PhD's+7 (on-going)
- Stays and collaborations: Groningen (The Netherlands), UCLA, KIAM (Russian Academy of Sciences), Stanford, Manchester (UK), Tsinghua (China), TokioTech (Japan), Napoli (Italy)...
- More info: www.fxtrias.com

About myself...

... and more personal stuff

- My complete name: Francesc Xavier Trias Miquel
- Born in Barcelona
- My mother tongue is Catalan but I also speak Spanish at native level.
- Hobbies? I like my work but also sports. Most practiced ones are running and football (the one you play with your feet ;-)):











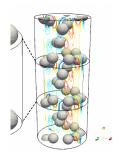
Barcelona (2019)

The CTTC research group

Heat and Mass Transfer Technological Center (Catalan: *Centre Tecnològic de Transferència de Calor*) has more than 25 years experience on CFD:

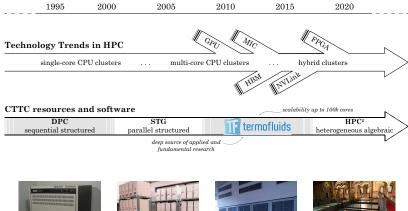
- Fundamental research on numerical methods, fluid dynamics and heat and mass transfer phenomena.
- **Applied research** on thermal and fluid dynamic optimization of thermal system and equipment.







CTTC's historical background in HPC

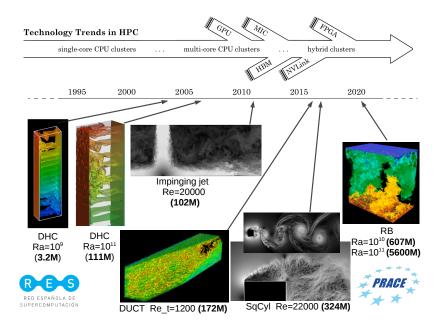












Let's begin with some math...

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Motivation

Soft landing...

$$\langle \nabla \cdot \vec{a} | \phi \rangle = -\langle \vec{a} | \nabla \phi \rangle$$

$$\langle \nabla^2 f | g \rangle = -\langle \nabla f | \nabla g \rangle = \langle f | \nabla^2 g \rangle$$

$$\langle C(\vec{u}, \phi_1) | \phi_2 \rangle = -\langle C(\vec{u}, \phi_2) | \phi_1 \rangle \quad \text{if} \quad \nabla \cdot \vec{u} = 0$$

$$\langle \nabla \times \vec{a} | \vec{b} \rangle = \langle \vec{a} | \nabla \times \vec{b} \rangle$$

Notation:

$$\langle a|b\rangle := \int_{\Omega} ab d\Omega$$
 $C(\vec{u}, \phi) := (\vec{u} \cdot \nabla) \phi$

REMEMBER: we always assume **no contribution from** domain boundary, $\partial \Omega$

00000000000000 00000

Operator symmetries and conservation

Kinetic energy (in 2D/3D)
$$\frac{1}{2} \frac{d \langle \vec{u} | \vec{u} \rangle}{dt} = \langle \frac{\partial \vec{u}}{\partial t} | \vec{u} \rangle = -\langle C(\vec{u}, \vec{u}) | \vec{u} \rangle + \nu \langle \nabla^2 \vec{u} | \vec{u} \rangle - \langle \nabla p | \vec{u} \rangle$$

$$= -\nu \langle \nabla \vec{u} | \nabla \vec{u} \rangle = -\nu ||\nabla \vec{u}||^2 \le 0$$

$$= -\nu \langle \nabla \times \nabla \times \vec{u} | \vec{u} \rangle = -\nu ||\omega||^2 \le 0$$

If v=0, then $\langle \vec{u}|\vec{u}\rangle$ remains constant!!! Also, if the flow is irrotational, $\vec{\omega} = \vec{0}$. Remember Bernoulli!

ADDITIONAL REMAINDER!!!

$$\nabla^2 \vec{u} = \nabla (\nabla \cdot \vec{u}) - \nabla \times \nabla \times \vec{u}$$

REMAINDER!!!

$$\begin{split} &\langle \nabla \cdot \vec{a} | \varphi \rangle \! = \! - \langle \vec{a} | \nabla \varphi \rangle \\ &\langle \nabla^2 f | g \rangle \! = \! - \langle \nabla f | \nabla g \rangle \! = \! \langle f | \nabla^2 g \rangle \\ &\langle C(\vec{u}, \varphi_1) | \varphi_2 \rangle \! = \! - \langle C(\vec{u}, \varphi_2) | \varphi_1 \rangle \quad \text{if} \quad \nabla \cdot \vec{u} \! = \! 0 \\ &\langle \nabla \times \vec{a} | \vec{b} \rangle \! = \! \langle \vec{a} | \nabla \! \times \! \vec{b} \rangle \end{split}$$

From Calculus to Algebra (C2A)

$$\langle a|b\rangle := \int_{\Omega} ab \, d\Omega \in \mathbb{R}$$

$$\langle a_h | b_h \rangle := a_h^T \mathbf{\Omega} b_h \in \mathbb{R}$$

$$a_{h} = \begin{vmatrix} a_{1} \\ a_{2} \\ a_{3} \\ a_{4} \\ a_{5} \\ a_{6} \end{vmatrix} \qquad \mathbf{\Omega} = \begin{vmatrix} \Omega_{1} & 0 & 0 & 0 & 0 & 0 \\ 0 & \Omega_{2} & 0 & 0 & 0 & 0 \\ 0 & 0 & \Omega_{3} & 0 & 0 & 0 \\ 0 & 0 & 0 & \Omega_{4} & 0 & 0 \\ 0 & 0 & 0 & 0 & \Omega_{5} & 0 \\ 0 & 0 & 0 & 0 & 0 & \Omega_{6} \end{vmatrix} \qquad b_{h} = \begin{vmatrix} b_{1} \\ b_{2} \\ b_{3} \\ b_{4} \\ b_{5} \\ b_{6} \end{vmatrix}$$

$$\langle a|b\rangle := \int_{\Omega} ab \, d\Omega \in \mathbb{R}$$

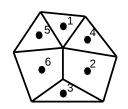
$$\langle a_h | b_h \rangle := a_h^T \mathbf{\Omega} b_h \in \mathbb{R}$$

$$a_{h} = \begin{vmatrix} a_{1} \\ a_{2} \\ a_{3} \\ a_{4} \\ a_{5} \\ a_{6} \end{vmatrix} \qquad \mathbf{\Omega} = \begin{vmatrix} \Omega_{1} & 0 & 0 & 0 & 0 & 0 \\ 0 & \Omega_{2} & 0 & 0 & 0 & 0 \\ 0 & 0 & \Omega_{3} & 0 & 0 & 0 \\ 0 & 0 & 0 & \Omega_{4} & 0 & 0 \\ 0 & 0 & 0 & 0 & \Omega_{5} & 0 \\ 0 & 0 & 0 & 0 & 0 & \Omega_{6} \end{vmatrix} \qquad b_{h} = \begin{vmatrix} b_{1} \\ b_{2} \\ b_{3} \\ b_{4} \\ b_{5} \\ b_{6} \end{vmatrix}$$

Soft landing...

$$\langle a|b\rangle := \int_{\Omega} ab \, d\Omega \in \mathbb{R}$$

$$\langle a_h | b_h \rangle := a_h^T \mathbf{\Omega} b_h \in \mathbb{R}$$



$$a_{h} = \begin{vmatrix} a_{1} \\ a_{2} \\ a_{3} \\ a_{4} \\ a_{5} \\ a_{6} \end{vmatrix} \qquad \mathbf{\Omega} = \begin{vmatrix} \Omega_{1} & 0 & 0 & 0 \\ 0 & \Omega_{2} & 0 & 0 \\ 0 & 0 & \Omega_{3} & 0 \\ 0 & 0 & 0 & \Omega_{4} \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{vmatrix}$$

$$b_{h} = \begin{vmatrix} b_{1} \\ b_{2} \\ b_{3} \\ b_{4} \\ b_{5} \\ b_{6} \end{vmatrix}$$

 Ω_6

$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = \nu \nabla^2 \vec{u} - \nabla p \qquad \nabla \cdot \vec{u} = 0$$

$$\Omega \frac{d u_h}{d t} + C(u_h) u_h = D u_h - \Omega G p_h \qquad M u_h = 0_h \qquad p_h(t) = \begin{vmatrix} p_1 \\ p_2 \\ p_3 \\ p_4 \end{vmatrix}$$

$$\nabla \cdot \vec{u} = 0$$

$$\mathbf{\Omega} \frac{d u_h}{d t} + C(u_h) u_h = \mathbf{D} u_h - \mathbf{\Omega} G p$$

$$\boldsymbol{M} u_h = 0_h \quad p_h(t) =$$

$$\begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ u_6 \end{bmatrix} u_h(t) = \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ u_6 \\ v_1 \\ v_2 \end{bmatrix}$$

 v_4

Soft landing...

$$T = \begin{vmatrix} \times & 0 & 0 & \times & \times & 0 \\ 0 & \times & \times & \times & 0 & \times \\ 0 & \times & \times & 0 & 0 & \times \\ \times & \times & 0 & \times & 0 & 0 \\ \times & 0 & 0 & 0 & \times & \times \\ 0 & \times & \times & 0 & \times & \times \end{vmatrix}$$

$$\mathbf{\Omega}_{u} = \mathbf{\Omega}_{v} = \begin{pmatrix} \mathbf{\Omega}_{1} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ 0 & \Omega_{2} & 0 & 0 & 0 & 0 \\ 0 & 0 & \Omega_{3} & 0 & 0 & 0 \\ 0 & 0 & 0 & \Omega_{4} & 0 & 0 \\ 0 & 0 & 0 & 0 & \Omega_{5} & 0 \\ 0 & 0 & 0 & 0 & 0 & \Omega \end{pmatrix}$$

$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = \nu \nabla^2 \vec{u} - \nabla p \qquad \nabla \cdot \vec{u} = 0$$

$$\mathbf{\Omega} \frac{d u_h}{d t} + C(u_h) u_h = \mathbf{D} u_h - \mathbf{\Omega} G p_h \qquad \mathbf{M} u_h = 0_h \qquad p_h(t) = \begin{vmatrix} p_1 \\ p_2 \\ p_3 \\ p_4 \end{vmatrix}$$

$$\nabla \cdot \vec{u} = 0$$

$$\Omega \frac{d u_h}{d t} + C(u_h) u_h = D u_h - \Omega G p$$

$$\mathbf{M} u_h = 0_h \quad p_h(a)$$

$$y_{\cdot}(t) = \begin{bmatrix} 1 & 1 & 1 \\ 1 & 1 & 1 \end{bmatrix}$$

U1

 v_2

Soft landing...

$$\mathbf{D} = \begin{pmatrix} \mathbf{D}_u & \\ & \mathbf{D}_v \end{pmatrix}$$

$$= \begin{pmatrix} d_{11} & 0 & 0 & d_{14} & d_{15} & 0 \\ 0 & d_{22} & d_{23} & d_{24} & 0 & d_{26} \\ 0 & d_{23} & d_{33} & 0 & 0 & d_{36} \\ d_{14} & d_{24} & 0 & d_{44} & 0 & 0 \\ d_{15} & 0 & 0 & 0 & d_{55} & d_{56} \\ 0 & d & d & 0 & d & d \end{pmatrix}$$

From Calculus to Algebra (C2A)

Motivation

U1 u_2

 V_1 v_2

 v_5

From Calculus to Algebra (C2A)

$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = v \nabla^2 \vec{u} - \nabla p \qquad \nabla \cdot \vec{u} = 0$$

$$\mathbf{\Omega} \frac{d u_h}{d t} + C(u_h) u_h = \mathbf{D} u_h - \mathbf{\Omega} \mathbf{G} p_h \qquad \mathbf{M} u_h = 0_h$$

$$\nabla \cdot \vec{u} = 0$$

$$p_1(t) = \begin{vmatrix} p_2 \\ p_3 \\ p_4 \\ p_5 \end{vmatrix}$$

Soft landing...

$$T = \begin{vmatrix} \times & 0 & 0 & \times & \times & 0 \\ 0 & \times & \times & \times & 0 & \times \\ 0 & \times & \times & 0 & 0 & \times \\ \times & \times & 0 & \times & 0 & 0 \\ \times & 0 & 0 & 0 & \times & \times \\ 0 & \times & \times & 0 & \times & \times \end{vmatrix}$$

$$\mathbf{G} = \begin{pmatrix} \mathbf{G}^x \\ \mathbf{G}^y \end{pmatrix}$$

$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = \nu \nabla^2 \vec{u} - \nabla p \qquad \nabla \cdot \vec{u} = 0$$

$$\mathbf{\Omega} \frac{d u_h}{d t} + \mathbf{C} (u_h) u_h = \mathbf{D} u_h - \mathbf{\Omega} \mathbf{G} p_h \qquad \mathbf{M} u_h = 0_h \qquad p_h(t) = \begin{vmatrix} p_1 \\ p_2 \\ p_3 \\ p_4 \end{vmatrix}$$

$$\mathbf{\Omega} \frac{d u_h}{d t} + \mathbf{C}(u_h) u_h = \mathbf{D} u_h - \mathbf{\Omega} \mathbf{G} p$$

$$\boldsymbol{M} \boldsymbol{u}_h = \boldsymbol{0}_h \quad \boldsymbol{p}_h(t) = \begin{bmatrix} \boldsymbol{k} \\ \boldsymbol{k} \end{bmatrix}$$

$$\begin{array}{c|c} & c_{14} = A_{14} U \\ & & c_{14} = A_{14} U \end{array}$$

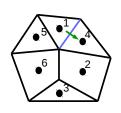
$$C = C =$$

$$C = \begin{pmatrix} C_u & \\ & C_v \end{pmatrix}$$

$$= \begin{pmatrix} c_{11} & 0 & 0 & c_{14} & c_{15} & 0 \\ 0 & c_{22} & c_{23} & c_{24} & 0 & c_{26} \\ 0 & c_{32} & c_{33} & 0 & 0 & c_{36} \\ c_{41} & c_{42} & 0 & c_{44} & 0 & 0 \\ c_{51} & 0 & 0 & 0 & c_{55} & c_{56} \\ 0 & c_{62} & c_{63} & 0 & c_{65} & c_{66} \end{pmatrix}$$

$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = v \nabla^2 \vec{u} - \nabla p \qquad \nabla \cdot \vec{u} = 0$

$$\mathbf{\Omega} \frac{d u_h}{d t} + C(u_h) u_h = \mathbf{D} u_h - \mathbf{\Omega} \mathbf{G} p_h \qquad \mathbf{M} u_h = 0_h$$



$$\mathbf{\Omega} = \begin{pmatrix} \mathbf{\Omega}_u & \\ & \mathbf{\Omega}_v \end{pmatrix}$$

$$\mathbf{M} = \begin{pmatrix} \mathbf{M}^u & \mathbf{M}^v \end{pmatrix}$$

$$T = \begin{pmatrix} \times & 0 & 0 & \times & \times & 0 \\ 0 & \times & \times & \times & 0 & \times \\ 0 & \times & \times & 0 & 0 & \times \\ \times & \times & 0 & \times & 0 & 0 \\ \times & \times & 0 & 0 & 0 & \times & \times \\ 0 & \times & \times & 0 & \times & \times \end{pmatrix}$$

$$C = \begin{pmatrix} C_u & \\ & C_v \end{pmatrix}$$

$$\mathbf{G} = \begin{pmatrix} \mathbf{G}^x \\ \mathbf{G}^y \end{pmatrix}$$

$$\mathbf{D} = \begin{pmatrix} \mathbf{D}_u & \\ & \mathbf{D}_v \end{pmatrix}$$

$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = \nu \nabla^2 \vec{u} - \nabla p \qquad \nabla \cdot \vec{u} = 0 \qquad \langle a|b \rangle := \int_{\Omega} ab \, d\Omega$$

$$\mathbf{\Omega} \frac{d \, u_h}{d \, t} + C(u_h) u_h = \mathbf{D} \, u_h - \mathbf{\Omega} \, G \, p_h \qquad \mathbf{M} \, u_h = 0_h \qquad \langle a_h | b_h \rangle := a_h^T \mathbf{\Omega} \, b_h$$

Let's consider the time evolution of $1/2\langle u_h|u_h\rangle...$

$$\frac{1}{2} \frac{d\langle u_h | u_h \rangle}{dt} = u_h^T \mathbf{\Omega} \frac{d u_h}{dt} = -u_h^T \mathbf{C}(u_h) u_h + u_h^T \mathbf{D} u_h - u_h^T \mathbf{\Omega} \mathbf{G} p_h$$
mimicking the properties

$$=u_h^T \mathbf{D} u_h \leq 0$$

...mimicking the properties of continuous NS egs leads to

REMAINDER!!!

$$\begin{split} \frac{1}{2} \frac{d \langle \vec{u} | \vec{u} \rangle}{dt} &= \langle \frac{\partial \vec{u}}{\partial t} | \vec{u} \rangle = -\langle C(\vec{u}, \vec{u}) | \vec{u} \rangle + v \langle \nabla^2 \vec{u} | \vec{u} \rangle - \langle \nabla p | \vec{u} \rangle \\ &= -v \langle \nabla \vec{u} | \nabla \vec{u} \rangle = -v | |\nabla \vec{u}||^2 \leq 0 \\ &= -v \langle \nabla \times \nabla \times \vec{u} | \vec{u} \rangle = -v ||\omega||^2 \leq 0 \end{split}$$

Numerical stability !!!

Algebraic operators

Soft landing...

$$\frac{1}{2} \frac{d\langle u_h | u_h \rangle}{dt} = u_h^T \mathbf{\Omega} \frac{d u_h}{dt} = -u_h^T \mathbf{C}(u_h) u_h + u_h^T \mathbf{D} u_h - u_h^T \mathbf{\Omega} \mathbf{G} p_h$$

$$= u_h^T \mathbf{D} u_h \le 0 , \quad \text{if } \mathbf{M} u_h = 0_h, \quad \forall u_h, p_h$$

$$u_h^T \mathbf{C}(u_h) u_h = 0 \longrightarrow \mathbf{C}(u_h) = -\mathbf{C}^T(u_h)$$

$$u_h^T \mathbf{\Omega} \mathbf{G} p_h = 0 \longrightarrow \mathbf{\Omega} \mathbf{G} = -\mathbf{M}^T$$

$$u_h^T \mathbf{D} u_h \le 0 \longrightarrow \mathbf{D} = \mathbf{D}^T \text{ def-}$$

REMAINDER!!!

$$\begin{split} \frac{1}{2} \frac{d \langle \vec{u} | \vec{u} \rangle}{dt} &= \langle \frac{\partial \vec{u}}{\partial t} | \vec{u} \rangle = -\langle C(\vec{u}, \vec{u}) | \vec{u} \rangle + \mathbf{v} \langle \nabla^2 \vec{u} | \vec{u} \rangle - \langle \nabla p | \vec{u} \rangle \\ &= -\mathbf{v} \langle \nabla \vec{u} | \nabla \vec{u} \rangle = -\mathbf{v} | \nabla \vec{u} |^2 \leq 0 \\ &= -\mathbf{v} \langle \nabla \times \nabla \times \vec{u} | \vec{u} \rangle = -\mathbf{v} | \mathbf{u} |^2 \leq 0 \end{split}$$

REMAINDER!!!

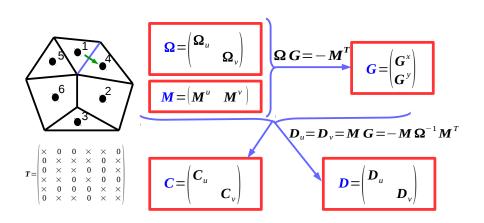
REMAINDER:::
$$\langle \nabla \cdot \vec{a} | \phi \rangle = -\langle \vec{a} | \nabla \phi \rangle$$

$$\langle \nabla^2 f | g \rangle = -\langle \nabla f | \nabla g \rangle = \langle f | \nabla^2 g \rangle$$

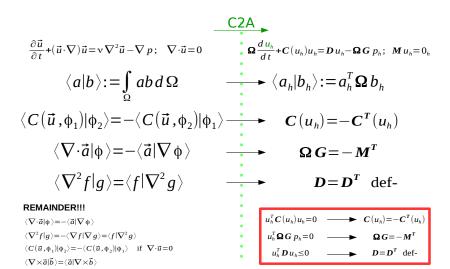
$$\langle C(\vec{u}, \phi_1) | \phi_2 \rangle = -\langle C(\vec{u}, \phi_2) | \phi_1 \rangle \quad \text{if } \nabla \cdot \vec{u} = 0$$

$$\langle \nabla \times \vec{a} | \dot{b} \rangle = \langle \vec{a} | \nabla \times \dot{b} \rangle$$

$$\mathbf{\Omega} \frac{d u_h}{d t} + C(u_h) u_h = \mathbf{D} u_h - \mathbf{\Omega} \mathbf{G} p_h \qquad \mathbf{M} u_h = 0_h$$

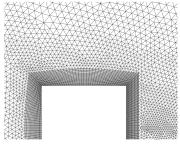


Soft landing...



Research question #1:

 Can we construct numerical discretizations of the Navier-Stokes equations suitable for complex geometries, such that the symmetry properties are exactly preserved?

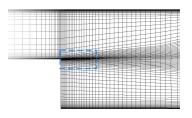


DNS¹ of the turbulent flow around a square cylinder at Re = 22000

¹F.X.Trias, A.Gorobets, A.Oliva. *Turbulent flow around a square cylinder at Reynolds number 22000: a DNS study*, **Computers&Fluids**, 123:87-98, 2015.

Research question #1:

 Can we construct numerical discretizations of the Navier-Stokes equations suitable for complex geometries, such that the symmetry properties are exactly preserved?

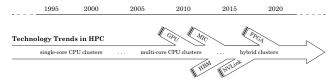


DNS² of backward-facing step at $Re_{\tau}=395$ and expansion ratio 2

 $^{^2}$ A.Pont-Vílchez, F.X.Trias, A.Gorobets, A.Oliva. *DNS of Backward-Facing Step flow at Re* $_{\tau} = 395$ *and expansion ratio 2.* **Journal of Fluid Mechanics**, 863:341-363, 2019.

Research question #2:

 How can we develop portable and efficient CFD codes for large-scale simulations on modern supercomputers?

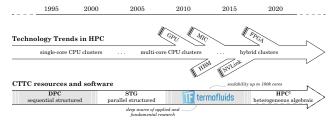


³X.Álvarez, A.Gorobets, F.X.Trias, R.Borrell, and G.Oyarzun. HPC² - a fully portable algebra-dominant framework for heterogeneous computing. Application to CFD. Computers & Fluids, 173:285-292, 2018

⁴ X.Álvarez, A.Gorobets, F.X.Trias. A hierarchical parallel implementation for heterogeneous computing. Application to algebra-based CFD simulations on hybrid supercomputers. **Computers & Fluids**. 214:104768, 2021.

Research question #2:

 How can we develop portable and efficient CFD codes for large-scale simulations on modern supercomputers?



HPC²: portable, algebra-based framework³ for heterogeneous computing is being developed⁴. Traditional stencil-based data and sweeps are replaced by algebraic structures (sparse matrices and vectors) and kernels. SpMM-based strategies to increase the arithmetic intensity are presented later...

 $^{^3}$ X.Álvarez, A.Gorobets, F.X.Trias, R.Borrell, and G.Oyarzun. HPC^2 - a fully portable algebra-dominant framework for heterogeneous computing. Application to CFD. **Computers & Fluids**, 173:285-292, 2018

⁴X.Álvarez, A.Gorobets, F.X.Trias. A hierarchical parallel implementation for heterogeneous computing. Application to algebra-based CFD simulations on hybrid supercomputers. **Computers & Fluids**. 214:104768, 2021.

Frequently used general purpose CFD codes:

• STAR-CCM+





ANSYS-FLUENT



Code-Saturne

OpenFOAM









Frequently used general purpose CFD codes:

STAR-CCM+





ANSYS-FLUENT ANSYS



Code-Saturne

OpenFOAM



Open FOAM®



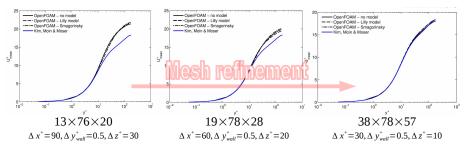


Main common characteristics of LES in such codes:

- Unstructured finite volume method, collocated grid
- Second-order spatial and temporal discretisation
- Eddy-viscosity type LES models

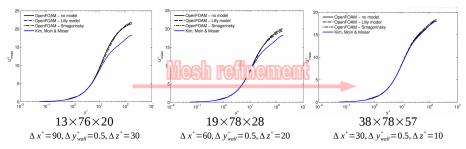
Soft landing..

Open ∇ FOAM® LES⁵ results of a turbulent channel for at $Re_{\tau}=180$



⁵E.M.J.Komen, L.H.Camilo, A.Shams, B.J.Geurts, B.Koren. A quantification method for numerical dissipation in quasi-DNS and under-resolved DNS, and effects of numerical dissipation in quasi-DNS and under-resolved DNS of turbulent channel flows, Journal of Computational Physics, 345, 565-595, 2017.

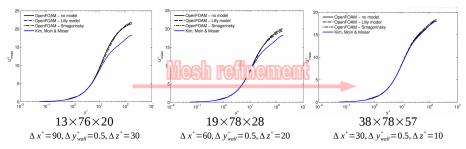
Open ∇ FOAM® LES⁵ results of a turbulent channel for at $Re_{\tau} = 180$



• Are LES results are merit of the SGS model?

⁵E.M.J.Komen, L.H.Camilo, A.Shams, B.J.Geurts, B.Koren. *A quantification method* for numerical dissipation in quasi-DNS and under-resolved DNS, and effects of numerical dissipation in quasi-DNS and under-resolved DNS of turbulent channel flows, **Journal of Computational Physics**, 345, 565-595, 2017.

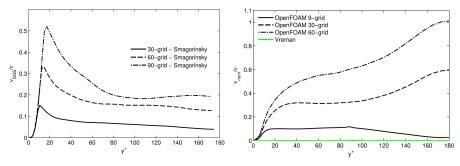
Open ∇ FOAM® LES⁵ results of a turbulent channel for at $Re_{\tau} = 180$



Are LES results are merit of the SGS model? Apparently NOT!!! X

⁵E.M.J.Komen, L.H.Camilo, A.Shams, B.J.Geurts, B.Koren. *A quantification method for numerical dissipation in quasi-DNS and under-resolved DNS, and effects of numerical dissipation in quasi-DNS and under-resolved DNS of turbulent channel flows, Journal of Computational Physics*, 345, 565-595, 2017.

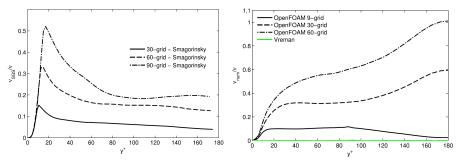
Open ∇ FOAM® LES⁶ results of a turbulent channel for at $Re_{\tau} = 180$



 $\nu_{num} \neq 0$

⁶E.M.J.Komen, L.H.Camilo, A.Shams, B.J.Geurts, B.Koren. *A quantification method for numerical dissipation in quasi-DNS and under-resolved DNS, and effects of numerical dissipation in quasi-DNS and under-resolved DNS of turbulent channel flows, Journal of Computational Physics*, 345, 565-595, 2017.

Open $\overline{ m V}$ FOAM ${ m ext{ iny ES}}^6$ results of a turbulent channel for at $Re_{ au}=180$



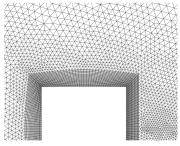
 $\nu_{SGS} < \nu_{num} \neq 0$

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Motivation

Research question #1:

 Can we construct numerical discretizations of the Navier-Stokes equations suitable for complex geometries, such that the symmetry properties are exactly preserved?



DNS¹ of the turbulent flow around a square cylinder at Re = 22000

¹F.X.Trias, A.Gorobets, A.Oliva. *Turbulent flow around a square cylinder at Reynolds number 22000: a DNS study,* **Computers&Fluids**, 123:87-98, 2015.

Continuous

$$\frac{\partial \mathbf{u}}{\partial t} + C(\mathbf{u}, \mathbf{u}) = \nu \nabla^2 \mathbf{u} - \nabla \rho$$
$$\nabla \cdot \mathbf{u} = 0$$

Continuous

$$\frac{\partial \mathbf{u}}{\partial t} + C(\mathbf{u}, \mathbf{u}) = \nu \nabla^2 \mathbf{u} - \nabla \mu$$
$$\nabla \cdot \mathbf{u} = 0$$

$$\frac{\partial \boldsymbol{u}}{\partial t} + C(\boldsymbol{u}, \boldsymbol{u}) = \nu \nabla^2 \boldsymbol{u} - \nabla p \qquad \Omega \frac{d\boldsymbol{u}_h}{dt} + C(\boldsymbol{u}_h) \boldsymbol{u}_h = \mathbf{D} \boldsymbol{u}_h - \mathbf{G} \boldsymbol{p}_h$$

$$\nabla \cdot \boldsymbol{u} = 0 \qquad \qquad \mathbf{M} \boldsymbol{u}_h = \mathbf{0}_h$$

Continuous

$$\frac{\partial \mathbf{u}}{\partial t} + C(\mathbf{u}, \mathbf{u}) = \nu \nabla^2 \mathbf{u} - \nabla p$$
$$\nabla \cdot \mathbf{u} = 0$$

$$\langle \boldsymbol{a}, \boldsymbol{b} \rangle = \int_{\Omega} \boldsymbol{a} \boldsymbol{b} d\Omega$$

$$\Omega \frac{d\mathbf{u}_h}{dt} + C(\mathbf{u}_h) \mathbf{u}_h = \mathbf{D}\mathbf{u}_h - G\mathbf{p}_h$$

$$M\mathbf{u}_h = \mathbf{0}_h$$

$$\langle \boldsymbol{a}_h, \boldsymbol{b}_h \rangle_h = \boldsymbol{a}_h^T \Omega \boldsymbol{b}_h$$

Soft landing...

Symmetry-preserving discretization

Continuous

$$\frac{\partial \mathbf{u}}{\partial t} + C(\mathbf{u}, \mathbf{u}) = \nu \nabla^2 \mathbf{u} - \nabla p$$
$$\nabla \cdot \mathbf{u} = 0$$

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$$\langle \boldsymbol{a}_h, \boldsymbol{b}_h \rangle_h = \boldsymbol{a}_h^T \Omega \boldsymbol{b}_h$$

$$C\left(\boldsymbol{u}_{h}\right)=-C^{T}\left(\boldsymbol{u}_{h}\right)$$

Soft landing...

Symmetry-preserving discretization

Continuous

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$$\langle \boldsymbol{a}_h, \boldsymbol{b}_h \rangle_h = \boldsymbol{a}_h^T \Omega \boldsymbol{b}_h$$

$$C(\boldsymbol{u}_h) = -C^T(\boldsymbol{u}_h)$$
$$\Omega_G^G = -M^T$$

Continuous

$$\frac{\partial \mathbf{u}}{\partial t} + C(\mathbf{u}, \mathbf{u}) = \nu \nabla^2 \mathbf{u} - \nabla p$$
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$$\Omega G = -M^T$$

$$D = D^T \quad def -$$

Why collocated arrangements are so popular?

STAR-CCM+



CD-adapco SIEMENS



ANSYS-FLUENT ANS



Code-Saturne



eDI

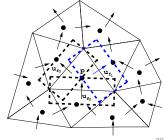


OpenFOAM

$$\Omega_{s} \frac{d\mathbf{u}_{s}}{dt} + C(\mathbf{u}_{s}) \mathbf{u}_{s} = \mathbf{D}\mathbf{u}_{s} - G\mathbf{p}_{c}; \quad \mathbf{M}\mathbf{u}_{s} = \mathbf{0}_{c}$$

In staggered meshes

- p-u_s coupling is naturally solved √
- \bullet C (u_s) and D difficult to discretize X



Why collocated arrangements are so popular?

STAR-CCM+



CD-adapco SIEMENS



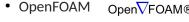
ANSYS-FLUENT





Code-Saturne

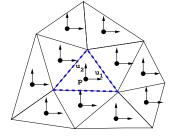




$$\Omega_c \frac{d\mathbf{u}_c}{dt} + C(\mathbf{u}_s) \mathbf{u}_c = \mathbf{D}\mathbf{u}_c - \mathbf{G}_c \mathbf{p}_c; \quad \mathbf{M}_c \mathbf{u}_c = \mathbf{0}_c$$

In collocated meshes

- p-uc coupling is cumbersome X
- C (u_s) and D easy to discretize √
- Cheaper, less memory,... √



Why collocated arrangements are so popular?

Everything is easy except the pressure-velocity coupling...

STAR-CCM+



CD-adapco SIEMENS



ANSYS-FLUENT





Code-Saturne

OpenFOAM



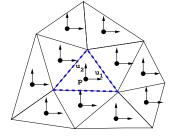
Open VFOAM®



$$\Omega_{c} \frac{d\mathbf{u}_{c}}{dt} + C(\mathbf{u}_{s}) \mathbf{u}_{c} = D\mathbf{u}_{c} - G_{c}\mathbf{p}_{c}; \quad M_{c}\mathbf{u}_{c} = \mathbf{0}_{c}$$

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- p-uc coupling is cumbersome X
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A vicious circle that cannot be broken...

Soft landing..

In summary⁷:

- Mass: $M\Gamma_{c\to s} \boldsymbol{u}_c = M\Gamma_{c\to s} \boldsymbol{u}_c L_c L^{-1} M\Gamma_{c\to s} \boldsymbol{u}_c \approx \boldsymbol{0}_c \boldsymbol{X}$
- Energy: $p_c (L L_c) p_c \neq 0 X$

⁷F.X.Trias, O.Lehmkuhl, A.Oliva, C.D.Pérez-Segarra, R.W.C.P.Verstappen. *Symmetry-preserving discretization of Navier-Stokes equations on collocated unstructured grids*, **Journal of Computational Physics**, 258 (1): 246-267, 2014.

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In summary⁷:

• Mass: $M\Gamma_{c \to s} \underline{u}_c = M\Gamma_{c \to s} \underline{u}_c - (L_c L^{-1}) M\Gamma_{c \to s} \underline{u}_c \approx \mathbf{0}_c X$

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• Energy: $\boldsymbol{p}_c (\mathsf{L} - \mathsf{L}_c) \boldsymbol{p}_c \neq 0 \ \boldsymbol{X}$

$$\tilde{\mathsf{L}} = \mathsf{L}_c$$
 Cleckerboard
$$p_c(\tilde{\mathsf{L}} - \mathsf{L}_c)p_c$$

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Motivation

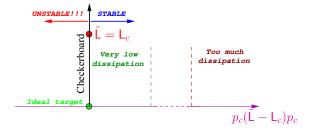
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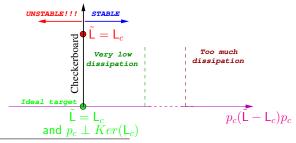
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In summary⁷:

• Mass:
$$M\Gamma_{c \to s} \boldsymbol{u_c} = M\Gamma_{c \to s} \boldsymbol{u_c} - \left[L_c L^{-1}\right] M\Gamma_{c \to s} \boldsymbol{u_c} \approx \boldsymbol{0_c} \boldsymbol{\chi}$$

• Energy: $p_c(L-L_c)p_c \neq 0$ X



⁷Shashank, J.Larsson, G.laccarino. *A co-located incompressible Navier-Stokes solver with exact mass, momentum and kinetic energy conservation in the inviscid limit,* **Journal of Computational Physics**, 229: 4425-4430,2010.

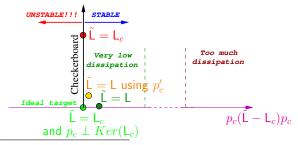
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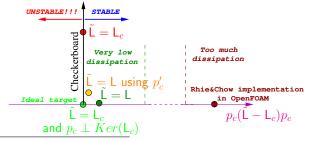
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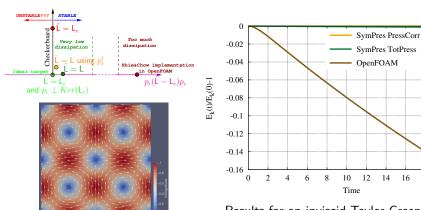
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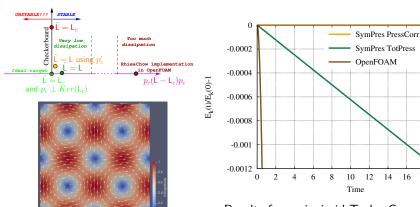
A vicious circle that cannot be broken can almost be broken...



Results for an inviscid Taylor-Green vortex⁸

⁸E.Komen, J.A.Hopman, E.M.A.Frederix, F.X.Trias, R.W.C.P.Verstappen. "A symmetry-preserving second-order time-accurate PISO-based method". **Computers & Fluids**, 225:104979, 2021.

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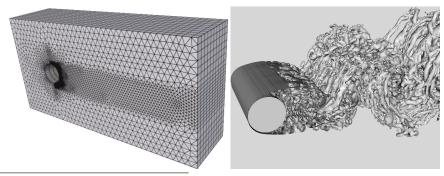
Results for an inviscid Taylor-Green vortex⁸

16

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Pressure-velocity coupling on collocated grids Examples of simulations

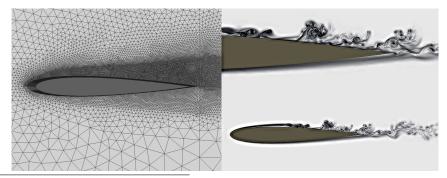
Despite these inherent limitations, symmetry-preserving collocated formulation has been successfully used for DNS/LES simulations⁹:



⁹R.Borrell, O.Lehmkuhl, F.X.Trias, A.Oliva. *Parallel Direct Poisson solver for discretizations with one Fourier diagonalizable direction.* **Journal of Computational Physics**, 230:4723-4741, 2011.

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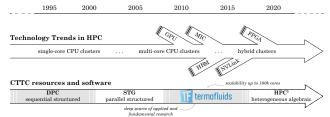


⁹F.X.Trias and O.Lehmkuhl. *A self-adaptive strategy for the time-integration of Navier-Stokes equations.* **Numerical Heat Transfer, part B**, 60(2):116-134, 2011.

Algebra-based approach naturally leads to portability

Research question #2:

 How can we develop portable and efficient CFD codes for large-scale simulations on modern supercomputers?



HPC²: portable, algebra-based framework for heterogeneous computing is being developed. Traditional stencil-based data and sweeps are replaced by algebraic structures (sparse matrices and vectors) and kernels. SpMM-based strategies to increase the arithmetic intensity are presented.

Algebra-based approach naturally leads to portability, to simple and analyzable formulations

Continuous

$$\frac{\partial \mathbf{u}}{\partial t} + C(\mathbf{u}, \mathbf{u}) = \nu \nabla^2 \mathbf{u} - \nabla \rho$$
$$\nabla \cdot \mathbf{u} = 0$$

$$\langle \boldsymbol{a}, \boldsymbol{b} \rangle = \int_{\Omega} \boldsymbol{a} \boldsymbol{b} d\Omega$$

$$\begin{split} \langle \mathcal{C} \left(\boldsymbol{u}, \varphi_1 \right), \varphi_2 \rangle &= - \langle \mathcal{C} \left(\boldsymbol{u}, \varphi_2 \right), \varphi_1 \rangle \\ \langle \nabla \cdot \boldsymbol{a}, \varphi \rangle &= - \langle \boldsymbol{a}, \nabla \varphi \rangle \\ \left\langle \nabla^2 \boldsymbol{a}, \boldsymbol{b} \right\rangle &= - \left\langle \boldsymbol{a}, \nabla^2 \boldsymbol{b} \right\rangle \end{split}$$

$$\Omega \frac{d\mathbf{u}_{h}}{dt} + C(\mathbf{u}_{h}) \mathbf{u}_{h} = \mathbf{D}\mathbf{u}_{h} - G\mathbf{p}_{h}$$
$$\mathbf{M}\mathbf{u}_{h} = \mathbf{0}_{h}$$

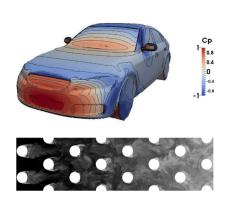
$$\langle \boldsymbol{a}_h, \boldsymbol{b}_h \rangle_h = \boldsymbol{a}_h^T \Omega \boldsymbol{b}_h$$

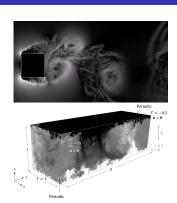
$$C(\boldsymbol{u}_h) = -C^T(\boldsymbol{u}_h)$$
$$\Omega G = -M^T$$

$$D = D^T$$
 def –

Soft landing...

Algebra-based approach naturally leads to portability, to simple and analyzable formulations and opens the door to new strategies¹⁰ to improve its perfomance...

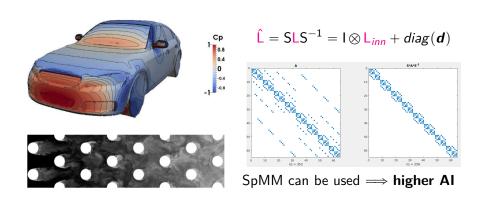




¹⁰ À.Alsalti-Baldellou, X.Álvarez-Farré, A.Oliva, F.X.Trias. Profiting spatial symmetries on solving the Poisson equation. Journal of Computational Physics (submitted)

Soft landing..

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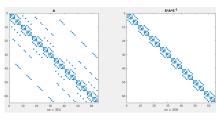
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Soft landing.

Benefits for Poisson solver are 3-fold:

- Higher arithmetic intensity (AI)
- Reduction of memory footprint
- Reduction in the number of iterations

$$\hat{\mathsf{L}} = \mathsf{SLS}^{-1} = \mathsf{I} \otimes \mathsf{L}_{inn} + diag(\boldsymbol{d})$$



SpMM can be used \Longrightarrow higher AI

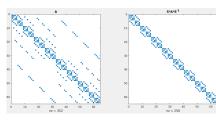
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Soft landing.

Benefits for Poisson solver are 3-fold:

- Reduction of memory footprint
- Reduction in the number of iterations
- \rightarrow Overall speed-up up to x2-x3 \checkmark
- → Memory reduction of \approx **2** \checkmark

$$\hat{\mathsf{L}} = \mathsf{SLS}^{-1} = \mathsf{I} \otimes \mathsf{L}_{inn} + diag(\mathbf{d})$$



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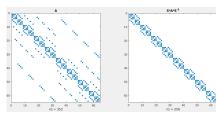
Other SpMM-based strategies to **increase AI** and **reduce memory** footprint:

- Multiple transport equations
- Parametric studies

Soft landing..

- Parallel-in-time simulations
- Go to higher-order?

$$\hat{\mathsf{L}} = \mathsf{SLS}^{-1} = \mathsf{I} \otimes \mathsf{L}_{inn} + diag(\mathbf{d})$$



SpMM can be used \Longrightarrow higher AI

¹⁰ A.Alsalti-Baldellou, X.Álvarez-Farré, A.Oliva, F.X.Trias. Profiting spatial symmetries on solving the Poisson equation.

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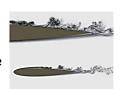
Concluding remarks

 Preserving symmetries either using staggered or collocated formulations is the key point for reliable LES/DNS simulations.



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- Main drawback of collocated formulations: you either have checkerboard or some (small) amount of artificial dissipation due to pressure term.





Concluding remarks

- Preserving symmetries either using staggered or collocated formulations is the key point for reliable LES/DNS simulations.
- Main drawback of collocated formulations: you either have checkerboard or some (small) amount of artificial dissipation due to pressure term.
- Algebra-based approach naturally leads to portability, to simple and analyzable formulations and opens the door to new strategies to improve its perfomance.

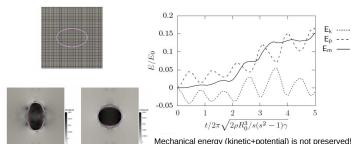






On-going (related) research

- **Rethinking** standard CFD operations (e.g. flux limiters¹¹, CFL,...) to adapt them into an algebraic framework (Motivation: maintaining a minimal number of basic kernels is crucial for portability!!!)
- Symmetry-preserving formulations for staggered unstructured grids
- ullet Symmetry-preserving formulations for **multiphase flows** 12

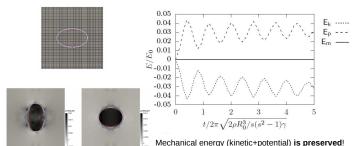


N.Valle, X.Álvarez, A.Gorobets, J.Castro, A.Oliva, F.X.Trias. On the implementation of flux limiters in algebraic frameworks. Computer Physics Communications, 271:108230, 2022

N.Valle, F.X.Trias, and J.Castro. An energy-preserving level set method for multiphase flows. Journal of Computational Physics, 400(1):108991, 2020 38 / 40

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- Symmetry-preserving formulations for multiphase flows¹²



 $^{^{11}}$ N.Valle, X.Álvarez, A.Gorobets, J.Castro, A.Oliva, F.X.Trias. On the implementation of flux limiters in algebraic frameworks. Computer Physics Communications, 271:108230, 2022

N.Valle, F.X.Trias, and J.Castro. An energy-preserving level set method for multiphase flows. Journal of Computational 38 / 40 Physics, 400(1):108991, 2020

Open questions and ideas for roundtable discussion

- Discrete conservation and turbulence modeling
 Reconciling numerics with subgrid-scale modeling, ILES, LES, DES, ...
- II. Are we satisfied with the existing SGS models for LES?

 Do we need better models? Is eddy-viscosity/eddy-diffusivity assumption good enough?
- III. What is (if it is) preventing LES/WMLES/Hybrid RANS-LES techniques to be routinely used in industrial applications? Robustness, computational cost, proper mesh generation, grey-area (or similar) issues,...
- IV. We can preserve (kinetic) energy. What about other inviscid invariants such as enstrophy (in 2D) or helicity?
- V. What about time-integration methods?

 We tend to ignore their effect. Shall we use symplectic time-integration methods?
- VI. Is it possible to preserve linear momentum in multiphase flows?



Conclusions